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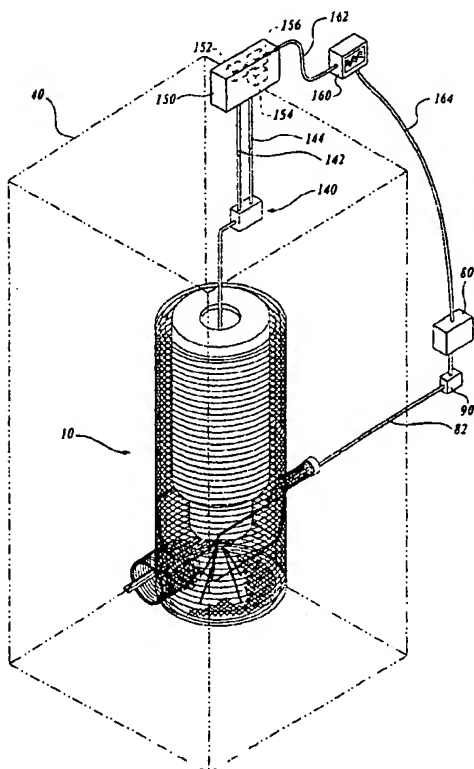
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(54) Title: SYSTEM AND METHOD FOR CHARACTERIZING A SAMPLE BY LOW-FREQUENCY SPECTRA



(57) Abstract: A method and apparatus for interrogating a sample that exhibits molecular rotation are disclosed. In practicing the method, the sample is placed in a container having both magnetic and electromagnetic shielding, and Gaussian noise is injected into the sample. An electromagnetic time-domain signal composed of sample source radiation superimposed on the injected Gaussian noise is detected, and this signal is used to generate a spectral plot that displays, at a selected power setting of the Gaussian noise source, low-frequency spectral components characteristic of the sample in a selected frequency range between DC and 50 kHz. In one embodiment, the spectral plot that is generated is a histogram of stochastic resonance events over the selected frequency range. From this spectrum, one or more low-frequency signal components that are characteristic of the sample being interrogated are identified.



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SYSTEM AND METHOD FOR CHARACTERIZING A SAMPLE BY LOW-FREQUENCY SPECTRA

CROSS-REFERENCE TO RELATED APPLICATIONS

[0001] This application is a continuation-in-part, and claims the benefit of, U.S. Patent Application No. 10/112,927, filed March 29, 2002, entitled APPARATUS AND METHOD FOR MEASURING MOLECULAR ELECTROMAGNETIC SIGNALS WITH A SQUID DEVICE AND STOCHASTIC RESONANCE TO MEASURE LOW-THRESHOLD SIGNALS (Attorney Docket No. 38547.8007.US00), International Patent Application No. PCT/US03/09544, filed March 28, 2003, entitled SYSTEM AND METHOD FOR CHARACTERIZING A SAMPLE BY LOW-FREQUENCY SPECTRA (Attorney Docket No. 38547.8005.WO00), and International Patent Application No. PCT/US03/11834, filed April 18, 2003, entitled SYSTEM AND METHOD FOR SAMPLE DETECTION BASED ON LOW-FREQUENCY SPECTRAL COMPONENTS (Attorney Docket No. 38547.8006.WO00), all incorporated herein by reference.

BACKGROUND

[0002] There are a variety of spectroscopic tools for characterizing atomic or molecular compound. These include, but are not limited to, x-ray, UV, visible-light, infrared and microwave spectroscopy, and nuclear and electron spin resonance (NMR and ESR) spectroscopy. In general, spectroscopic tools are useful for at least four different type of chemical-analytical problems: first, to characterize an atomic and molecular compound according to its spectrographic features, e.g., spectral components; second, to determine the atomic composition of a compound, according to the spectral characteristics of atoms making up the compound; third, to determine 2-D or 3-D conformation of a molecular compound according to the spectral characteristic of atom-atom interactions in the compound; and fourth, to detect and identify components, e.g., contaminants, in a sample according to the distinguishing spectral characteristics of the compound being detected.

[0003] Most existing spectroscopic tools provide some unique advantage(s) in terms of sensitivity, the information gained, ease of measurement and cost. Because each tool provides information not otherwise available, it is generally advantageous to be able to bring to bear on any chemical-analytical, as many pertinent spectroscopic tools as possible.

## SUMMARY

[0004] The invention includes, in one aspect, a method of characterizing spectral emission features of a sample material, e.g., low-frequency emissions related to molecular motion within the sample. The method uses a time-domain signal of the sample over a sample-duration time  $T$ , and a sampling rate  $F$  for sampling the time domain signal, where  $F * T$  is the total sample count  $S$ ,  $F$  is approximately twice the frequency domain resolution  $f$  of a Real Fast Fourier Transform of the time-domain signal sampled at sampling rate  $F$ , and  $S > f * n$ , where  $n$  is at least 10. The program selects  $S/n$  samples from the stored time domain signal and performs a Real Fast Fourier Transform (RFFT) on the samples. The RFFT is then normalized (e.g., by setting the highest value to 1), and an average power for the signal is calculated from the normalized signal. Next, the program places an event count in each of  $f$  selected-frequency event bins, where the measured power at the corresponding selected frequency  $\geq$  average power  $* \epsilon$  obtains, where  $0 < \epsilon < 1$ , and  $\epsilon$  is chosen such that the total number of counts placed in an event bin is between about 20-50% of the maximum possible bin counts in that bin. These steps are repeated  $n$  times, generating a histogram that shows, for each event bin  $f$  over a selected frequency range, the number of event counts in each bin.

[0005] The method may further include the step of placing the normalized power value from the RFFT in  $f$  corresponding-frequency power bins, and, after  $n$  cycles of program operation, (a) dividing the accumulated values placed in each of the  $f$  power bins by  $n$ , to yield an average power in each bin, and (b) displaying on the histogram, the average power in each bin. The method may further include identifying those bins in the histogram that have an event count above a given threshold and an average power.

[0006] Also disclosed is a low-frequency spectral signature associated with a material of interest comprising a list of frequency components in the DC-50 kHz

frequency range that are generated by the above method. The frequencies in the list may be identified from a histogram of the number of sample-dependent stochastic events occurring at each of a plurality of spectral increments within a selected frequency range between DC and 50 kHz.

[0007] In another aspect, the invention includes an apparatus for interrogating a sample that exhibits low-frequency molecular motion. The apparatus includes a magnetically and electromagnetically shielded container adapted for receiving the sample, an adjustable-power source of Gaussian noise for injection into the sample, with the sample in said container, and a detector for detecting an electromagnetic time-domain signal composed of sample source radiation superimposed on the injected Gaussian noise. An electronic computer in the apparatus receives the time-domain signal from the detector, and processes the signal to generate a spectral plot that displays, at a selected power setting of the Gaussian noise source, low-frequency spectral components characteristic of the sample in a selected frequency range between DC and 50 kHz.

[0008] In one general embodiment, the electronic computer includes a signal analyzer that functions to (i) calculate a series of Fourier spectra of the time-domain signal over each of a plurality of defined time periods, in a selected frequency range between DC and 50 kHz, and (ii) average the Fourier spectra.

[0009] Typically, at least five Fourier spectra are calculated, each taken over a 1-5 second time-domain interval.

[0010] In another general embodiment, the electronic computer includes machine-readable code operable to carry out the method described above for generating a histogram of spectral events.

[0011] The source of Gaussian noise in the apparatus may be an adjustable-power Gaussian noise generator and a Helmholtz coil which is contained within the magnetic cage and the Faraday cage, and which receives a selected noise output signal from the noise generator in the range 100 mV to 1 V. The injector is designed to inject Gaussian noise into the sample at a frequency, for example, between DC and 8 kHz.

[0012] The detector in the apparatus may be a first-derivative superconducting gradiometer which outputs a current signal, and a SQUID operatively connected to the gradiometer to convert the current signal to an amplified voltage signal.

[0013] The container in the apparatus may include an attenuation tube having a sample-holding region, a magnetic shielding cage surrounding the region, and a Faraday cage contained within the magnetic shielding cage and also surrounding the region. In this embodiment, the source of Gaussian noise may include a Gaussian noise generator and a Helmholtz coil which is contained within the magnetic cage and the Faraday cage, and which receives a noise output signal from the noise generator, and which further includes, for use in removing stationary noise components in the time-dependent signal, a signal inverter operatively connected to the said noise source and to said SQUID, for receiving Gaussian noise from the noise source and outputting into said SQUID, Gaussian noise in inverted form with respect to the Gaussian noise injected into the sample.

[0014] In still another aspect, the invention includes a method for interrogating a sample that exhibits low-frequency molecular motion. In practicing the method, the sample is placed in a container having both magnetic and electromagnetic shielding, and Gaussian noise is injected into the sample at a selected noise amplitude. An electromagnetic time-domain signal composed of sample source radiation superimposed on the injected Gaussian noise, is recorded, and from this, a spectral plot that contains, at a selected power setting of the Gaussian noise source, low-frequency, sample-dependent spectral components characteristic of the sample in a selected frequency range between DC and 50 kHz is generated. The steps are repeated at different selected noise amplitudes until a plot showing a maximum or near maximum number of spectral components characteristic of the sample are generated.

[0015] In one embodiment, the spectral plot is generated by (i) calculating a series of Fourier spectra of the time-domain signal over each of a plurality of defined time periods, in a selected frequency range between DC and 50 kHz, and (ii) averaging the Fourier spectra.

[0016] In another general embodiment, the spectral plot is generated by the histogram method above.

[0017] These and other objects and features of the invention will become more fully apparent when the following detailed description of the invention is read in conjunction with the accompanying drawings.

## BRIEF DESCRIPTION OF THE DRAWINGS

[0018] Figure 1 is an isometric view of one embodiment of a molecular electromagnetic signaling detection apparatus formed in accordance with one embodiment of the present invention;

[0019] Figure 2 is an enlarged, detail view of the faraday cage and its contents shown in Figure 1; and

[0020] Figure 3 is an enlarged, cross sectional view of one of the attenuation tubes shown in Figures 1 and 2.

[0021] Figure 4 is a cross-section view of the faraday cage and its contents shown in Figure 2.

[0022] Figure 5 is a cross-section view of an alternative embodiment of the invention shown in Figures 1 through 4.

[0023] Figure 6 is an enlarged, detail view of the frames supporting the coils of the Helmholtz transformer described herein.

[0024] Figure 7 is a diagram of an alternative electromagnetic emission detection system.

[0025] Figure 8 diagram of the processing unit included in the detection system of the above Figures.

[0026] Figure 9 is a diagram of an alternative processing unit to that of Figure 8.

[0027] Figure 10 is a flow diagram of the signal detection and processing performed by the present system.

[0028] Figure 11A is a spectral plot of the emissions of a first sample.

[0029] Figure 11B is spectral plot of the emissions of a second sample.

[0030] Figures 12A and 12B are spectral plots, in the spectral region between 500-530 Hz, for a sample of saturated NaCl, generated by Fourier transforming a non-correlated time-domain sample signal (12A), and Fourier transforming a cross-correlated sample spectrum (12B).

[0031] Figures 13A and 13B are spectral plots, in the spectral region between 500-530 Hz, for a sample of alkyl ether sulfate, generated by Fourier transforming a non-correlated time-domain sample signal (13A), and Fourier transforming a cross-correlated sample spectrum (13B).

[0032] Figures 14A-14F are spectral plots, in the spectral region between 500-530 Hz, for samples of deionized water (14A), a saturated NaCl solution (14B), a solution of 1% NaCl in deionized water (14C); a saturated NaBr sample (14D), alkyl ether sulfate in deionized water (14E), and no sample (14F).

[0033] Figures 15A-15F are spectral plots, in the spectral region between 500 and 535Hz, of a sample of an amino acid at a 1:100 wt/volume solution (15A) and at increasing w/v dilutions of 1:10,000 (15B), 1:1 million (15C), 1:100 million (15D), 1:10 billion (15E and 15F), where the spectra in Figures 15A-15E were generated with 50 second recordings and 40 minute correlations, and the spectrum of Figure 15F was generated with a 4:25 minute recording with a 12 hour correlation.

[0034] Figure 16 is a schematic diagram illustrating an alternative embodiment of a molecular electromagnetic signaling detection apparatus.

[0035] Figure 17A is a cross-sectional view of the alternative embodiment of Figure 16.

[0036] Figure 17B is an enlargement of a portion of Figure 17A.

[0037] Figure 18 is a cross-sectional isometric view of Figure 17B.

[0038] Figure 19 is a diagram of an alternative processing unit to that of Figure 9.

[0039] Figure 20 shows a high-level flow diagram of data flow for the histogram spectral plot method of the invention;

[0040] Figure 21 is a flow diagram of the algorithm for generating a spectral plot histogram, in accordance with the invention, and

[0041] Figures 22A-22D are histogram spectra of a sample taken at four different noise power levels.

[0042] Figures 23A-23C are computer screen shots displaying a user interface for generating and displaying a spectral plot histogram, with Figure 23C being in color.

[0043] Figure 24 is a schematic drawing of an embodiment of an electromagnetic emission detection system similar to that of Figures 8, 16 and 19.

[0044] Figure 25 is a schematic diagram illustrating a first alternative embodiment to the system of Figure 24.

[0045] Figure 26 is a schematic diagram of a second alternative embodiment to the system of Figure 24.

[0046] Figure 27 is a partial schematic, partial block diagram of a third alternative embodiment to the system of Figure 24.

[0047] In the drawings, identical reference numbers identify identical or substantially similar elements or acts. To easily identify the discussion of any particular element or act, the most significant digit or digits in a reference number refer to the Figure number in which that element is first introduced.

## DETAILED DESCRIPTION

### I. Definitions

[0048] The terms below have the following definitions unless indicated otherwise.

[0049] "Sample that exhibits molecular rotation" refers to a sample material, which may be in gaseous, liquid or solid form (other than a solid metal) in which one or more of the molecular compounds or atomic ions making up or present in the sample exhibit rotation.

[0050] "Magnetic shielding" refers to shielding that inhibits or prevents passage of magnetic flux as a result of the magnetic permeability of the shielding material.

[0051] "Electromagnetic shielding" refers to, e.g., standard Faraday electromagnetic shielding.

[0052] "Time-domain signal" or "time-series signal" refers to a signal with transient signal properties that change over time.

[0053] "Sample-source radiation" refers to magnetic flux emissions resulting from molecular motion of a sample, such as the rotation of a molecular dipole in a magnetic field.

[0054] "Gaussian noise" means random noise having a Gaussian power distribution.

[0055] "Stationary white Gaussian noise" means random Gaussian noise that has no predictable future components.

[0056] "Frequency-domain spectrum" refers to a Fourier frequency plot of a time-domain signal.

[0057] "Spectral components" refer to singular or repeating qualities within a time-domain signal that can be measured in the frequency, amplitude, and/or phase

domains. Spectral components will typically refer to signals present in the frequency domain.

[0058] "Similar sample," with reference to a first sample, refers to the same sample or a sample having substantially the same sample components as the first sample.

[0059] "Faraday cage" refers to an electromagnetic shielding configuration that provides an electrical path to ground for unwanted electromagnetic radiation, thereby quieting an electromagnetic environment.

## II. Apparatus

[0060] Described in detail below is a system and method for detecting, processing, and presenting low frequency electromagnetic emissions or signals of a sample of interest. In one embodiment, a known white or Gaussian noise signal is introduced to the sample. The Gaussian noise is configured to permit the electromagnetic emissions from the sample to be sufficiently detected by a signal detection system. Sets of detected signals are processed together to ensure repeatability and statistical relevance. The resulting emission pattern or spectrum can be displayed, stored, and/or identified as a particular substance.

[0061] The following description provides specific details for a thorough understanding of, and enabling description for, embodiments of the invention. However, one skilled in the art will understand that the invention may be practiced without these details. In other instances, well-known structures and functions have not been shown or described in detail to avoid unnecessarily obscuring the description of embodiments of the invention.

[0062] As explained in detail below, embodiments of the present invention are directed to providing an apparatus and method for the repeatable detection and recording of low-threshold molecular electromagnetic signals. A magnetically shielded faraday cage shields the sample material and detection apparatus from extraneous electromagnetic signals. Within the magnetically shielded faraday cage, a coil injects white or Gaussian noise, a nonferrous tray holds the sample, and a gradiometer detects low-threshold molecular electromagnetic signals. The apparatus further includes a superconducting quantum interference device ("SQUID") and a preamplifier.

[0063] The apparatus is used by placing a sample within the magnetically shielded faraday cage in close proximity to the noise coil and gradiometer. White noise is injected through the noise coil and modulated until the molecular electromagnetic signal is enhanced through stochastic resonance. The enhanced molecular electromagnetic signal, shielded from external interference by the faraday cage and the field generated by the noise coil, is then detected and measured by the gradiometer and SQUID. The signal is then amplified and transmitted to any appropriate recording or measuring equipment.

[0064] Referring to Figure 1, there is shown a shielding structure 10 which includes, in an outer to inner direction, a conductive wire cage 16 which is a magnetic shield and inner conductive wire cages 18 and 20 which provide electromagnetic shielding. In another embodiment, the outer magnetic shield is formed of a solid aluminum plate material having an aluminum-nickel alloy coating, and the electromagnetic shielding is provided by two inner wall structures, each formed of solid aluminum.

[0065] Referring to Figure 2, the faraday cage 10 is open at the top, and includes side openings 12 and 14. The faraday cage 10 is further comprised of three copper mesh cages 16, 18 and 20, nestled in one another. Each of the copper mesh cages 16, 18 and 20 is electrically isolated from the other cages by dielectric barriers (not shown) between each cage.

[0066] Side openings 12 and 14 further comprise attenuation tubes 22 and 24 to provide access to the interior of the faraday cage 10 while isolating the interior of the cage from external sources of interference. Referring to Figure 3, attenuation tube 24 is comprised of three copper mesh tubes 26, 28 and 30, nestled in one another. The exterior copper mesh cages 16, 18 and 20 are each electrically connected to one of the copper mesh tubes 26, 28 and 30, respectively. Attenuation tube 24 is further capped with cap 32, with the cap having hole 34. Attenuation tube 22 is similarly comprised of copper mesh tubes 26, 28 and 30, but does not include cap 32.

[0067] Referring again to Figure 2, a low-density nonferrous sample tray 50 is mounted in the interior of the faraday cage 10. The sample tray 50 is mounted so that it may be removed from the faraday cage 10 through the attenuation tube 22 and side opening 12. Three rods 52, each of which is greater in length than the distance from the center vertical axis of the faraday cage 10 to the outermost edge of

the attenuation tube 22, are attached to the sample tray 50. The three rods 52 are adapted to conform to the interior curve of the attenuation tube 22, so that the sample tray 50 may be positioned in the center of the faraday cage 10 by resting the rods in the attenuation tube. In the illustrated embodiment, the sample tray 50 and rods 52 are made of glass fiber epoxy. It will be readily apparent to those skilled in the art that the sample tray 50 and rods 52 may be made of other nonferrous materials, and the tray may be mounted in the faraday cage 10 by other means, such as by a single rod.

[0068] Referring again to Figure 2, mounted within the faraday cage 10 and above the sample tray 50 is a cryogenic dewar 100. In the disclosed embodiment, the dewar 100 is adapted to fit within the opening at the top of faraday cage 10 and is a Model BMD-6 Liquid Helium Dewar manufactured by Tristan Technologies, Inc. The dewar 100 is constructed of a glass-fiber epoxy composite. A gradiometer 110 with a very narrow field of view is mounted within the dewar 100 in position so that its field of view encompasses the sample tray 50. In the illustrated embodiment, the gradiometer 110 is a first order axial detection coil, nominally 1 centimeter in diameter, with a 2 % balance, and is formed from a superconductor. The gradiometer can be any form of gradiometer excluding a planar gradiometer. The gradiometer 110 is connected to the input coil of one low temperature direct current superconducting quantum interference device ("SQUID") 120. In the disclosed embodiment, the SQUID is a Model LSQ/20 LTS dc SQUID manufactured by Tristan Technologies, Inc. It will be recognized by those skilled in the art that high temperature or alternating current SQUIDs can be used without departing from the spirit and scope of the invention. In an alternative embodiment, the SQUID 120 includes a noise suppression coil 124.

[0069] The disclosed combination of gradiometer 110 and SQUID 120 have a sensitivity of 5 microTesla/ $\sqrt{\text{Hz}}$  when measuring magnetic fields.

[0070] The output of SQUID 120 is connected to a Model SP Cryogenic Cable 130 manufactured by Tristan Technologies, Inc. The Cryogenic Cable 130 is capable of withstanding the temperatures within and without the dewar 100 and transfers the signal from the SQUID 120 to Flux-Locked Loop 140, which is mounted externally to the faraday cage 10 and dewar 100. The Flux-Locked Loop 140 in the

disclosed embodiment is an iFL-301-L Flux Locked Loop manufactured by Tristan Technologies, Inc.

[0071] Referring to Figure 1, the Flux Locked Loop 140 further amplifies and outputs the signal received from the SQUID 120 via high-level output circuit 142 to an iMC-303 iMAG® SQUID controller 150. The Flux-Locked Loop 140 is also connected via a model CC-60 six-meter fiber-optic composite connecting cable 144 to the SQUID controller 150. The fiber-optic connecting cable 144 and SQUID controller 150 are manufactured by Tristan Technologies, Inc. The controller 150 is mounted externally to the magnetic shielding cage 40. The fiber-optic connecting cable 144 carries control signals from the SQUID controller 150 to the Flux Locked Loop 140, further reducing the possibility of electromagnetic interference with the signal to be measured. It will be apparent to those skilled in the art that other Flux-Locked Loops, connecting cables, and Squid controllers can be used without departing from the spirit and scope of the invention.

[0072] The SQUID controller 150 further comprises high resolution analog to digital converters 152, a standard GP-IB bus 154 to output digitalized signals, and BNC connectors 156 to output analog signals. In the illustrated embodiment, the BNC connectors are connected to a dual trace oscilloscope 160 through patch cord 162.

[0073] Referring to Figure 2, a two-element Helmholtz transformer 60 is installed to either side of the sample tray 50 when the sample tray is fully inserted within the faraday cage 10. In the illustrated embodiment, the coil windings 62 and 64 of the Helmholtz transformer 60 are designed to operate in the direct current to 50 kilohertz range, with a center frequency of 25 kilohertz and self-resonant frequency of 8.8 megahertz. In the illustrated embodiment, the coil windings 62 and 64 are generally rectangular in shape and are approximately 8 inches tall by 4 inches wide. Other Helmholtz coil shapes may be used but should be shaped and sized so that the gradiometer 110 and sample tray 50 are positioned within the field produced by the Helmholtz coil. Each of coil windings 62 and 64 is mounted on one of two low-density nonferrous frames 66 and 68. The frames 66 and 68 are hingedly connected to one another and are supported by legs 70. Frames 66 and 68 are slidably attached to legs 70 to permit vertical movement of the frames in relation to the lower portion of dewar 100. Movement of the frames permits adjustment of the coil windings 62 and 64 of the Helmholtz transformer 60 to vary the amplitude of white

noise received at gradiometer 110. The legs 70 rest on or are epoxied onto the bottom of the faraday cage 10. In the illustrated embodiment, the frames 66 and 68 and legs 70 are made of glass fiber epoxy. Other arrangements of transformers or coils may be used around the sample tray 50 without departing from the spirit and scope of the invention.

[0074] Referring to Figure 4, there is shown a cross-sectional view of the faraday cage and its contents, showing windings 62 of Helmholtz transformer 60 in relation to dewar 100 and faraday cage 10. Note also in Figure 4 the positioning of sample tray 50 and sample 200.

[0075] Referring to Figure 5, there is shown an alternative embodiment in which the Helmholtz coil windings 62 and 64 are fixed in a vertical orientation and an additional noise coil 300 is positioned below sample tray 50. The windings of the additional noise coil 300 are substantially perpendicular to the vertical windings 62 and 64 of Helmholtz transformer 60, and the windings of the additional noise coil 300 are thus substantially in parallel orientation to the bottom of faraday cage 10.

[0076] In this alternative embodiment, noise would be fed to noise coil 300 from an identical twisted pair wire (not shown) as that supplying the Helmholtz coil. The noise source would originate with the same noise generator used to supply noise to the Helmholtz coil. Noise would be sampled either at the noise generator via an additional noise output connection, or via a balanced splitter from an output connection to the noise generator. Attenuation of the noise signal at additional noise coil 300 would be through an adjustable RF signal attenuation circuit, of which many are available commercially, or via a suitable series of fixed value RF attenuation filters.

[0077] Referring to Figure 6, a detail of the frames supporting the coils of Helmholtz transformer 60 may be seen; the reference point of Figure 6 is 90 degrees from the view of Figure 4, and omits the faraday cage 10. Frames 66 and 68 are disposed to show the coil windings of the Helmholtz coil in a substantially vertical position and parallel to one another. Frames 66' and 68' illustrate the rotation of said frames about the axis of the hinged connection joining said frames, so as to dispose the coil windings of the Helmholtz transformer in a non-parallel relationship with one another.

[0078] Referring again to Figure 1, an amplitude adjustable white noise generator 80 is external to magnetic shielding cage 40, and is electrically connected

to the Helmholtz transformer 60 through filter 90 by electrical cable 82. Referring to Figure 3, cable 82 is run through side opening 12, attenuation tube 24, and through cap 32 via hole 34. Cable 82 is a co-axial cable further comprising a twisted pair of copper conductors 84 surrounded by interior and exterior magnetic shielding 86 and 88, respectively. In other embodiments, the conductors can be any nonmagnetic electrically conductive material, such as silver or gold. The interior and exterior magnetic shielding 86 and 88 terminates at cap 32, leaving the twisted pair 84 to span the remaining distance from the end cap to the Helmholtz transformer 60 shown in Figure 1. The interior magnetic shielding 86 is electrically connected to Faraday cage 16 through cap 32, while the exterior magnetic shielding is electrically connected to the magnetically shielded cage 40 shown in Figure 1.

[0079] Referring to Figure 1, the white noise generator 80 can generate nearly uniform noise across a frequency spectrum from zero to 100 kilohertz. In the illustrated embodiment, the filter 90 filters out noise above 50 kilohertz, but other frequency ranges may be used without departing from the spirit and scope of the invention.

[0080] White noise generator 80 is also electrically connected to the other input of dual trace oscilloscope 160 through patch cord 164.

[0081] Referring to Figures 1, 2 and 3, a sample of the substance 200 to be measured is placed on the sample tray 50 and the sample tray is placed within the Faraday cage 10. In the first embodiment, the white noise generator 80 is used to inject white noise through the Helmholtz transformer 60. The noise signal creates an induced voltage in the gradiometer 110. The induced voltage in the gradiometer 110 is then detected and amplified by the SQUID 120, the output from the SQUID is further amplified by the flux locked loop 140 and sent to the SQUID controller 150, and then sent to the dual trace oscilloscope 160. The dual trace oscilloscope 160 is also used to display the signal generated by white noise generator 80.

[0082] The white noise signal is adjusted by altering the output of the white noise generator 80 and by rotating the Helmholtz transformer 60 around the sample 200, shown in Figure 2. Rotation of the Helmholtz transformer 60 about the axis of the hinged connection of frames 66 and 68 alters its phasing with respect to the gradiometer 110. Depending upon the desired phase alteration, the hinged connection of frames 66 and 68 permits windings 62 and 64 to remain parallel to one another while rotating approximately 30 to 40 degrees around sample tray 50. The

hinged connection also permits windings 62 and 64 to rotate as much as approximately 60 degrees out of parallel, in order to alter signal phasing of the field generated by Helmholtz transformer 60 with respect to gradiometer 110. The typical adjustment of phase will include this out-of-parallel orientation, although the other orientation may be preferred in certain circumstances, to accommodate an irregularly shaped sample 200, for example. Noise is applied and adjusted until the noise is 30 to 35 decibels above the molecular electromagnetic emissions sought to be detected. At this noise level, the noise takes on the characteristics of the molecular electromagnetic signal through the well-known phenomenon of stochastic resonance. The stochastic product sought is observed when the oscilloscope trace reflecting the signal detected by gradiometer 110 varies from the trace reflecting the signal directly from white noise generator 80. In alternative embodiments, the signal can be recorded and or processed by any commercially available equipment.

[0083] In an alternative embodiment, the method of detecting the molecular electromagnetic signals further comprises injecting noise 180° out of phase with the original noise signal applied at the Helmholtz transformer 60 through the noise suppression coil 124 of the SQUID 120. The stochastic product sought can then be observed when the oscilloscope trace reflecting the signal detected by gradiometer 110 becomes non-random.

[0084] Regardless of how the noise is injected and adjusted, the stochastic product can also be determined by observing when an increase in spectral peaks occurs. The spectral peaks can be observed as either a line plot on oscilloscope 160 or as numerical values, or by other well known measuring devices.

[0085] Embodiments of the present invention provide a method and apparatus for detecting extremely low-threshold molecular electromagnetic signals without external interference. They further provide for the output of those signals in a format readily usable by a wide variety of signal recording and processing equipment.

[0086] Referring now to Figure 7, an alternative embodiment to the molecular electromagnetic emission detection and processing system of the above Figures is shown. A system 700 includes a detection unit 702 coupled to a processing unit 704. Although the processing unit 704 is shown external to the detection unit 702, at least a part of the processing unit can be located within the detection unit.

[0087] The detection unit 702, which is shown in a cross-sectional view in Figure 7, includes a plurality of components nested or concentric with each other. A sample chamber or faraday cage 706 is nested within a metal cage 708. Each of the sample chamber 706 and the metal cage 708 can be comprised of aluminum material. The sample chamber 706 can be maintained in a vacuum and may be temperature controlled to a preset temperature. The metal cage 708 is configured to function as a low pass filter.

[0088] Between the sample chamber 706 and the metal cage 708 and encircling the sample chamber 706 are a set of parallel heating coils or elements 710. One or more temperature sensor 711 is also located proximate to the heating elements 710 and the sample chamber 706. For example, four temperature sensors may be positioned at different locations around the exterior of the sample chamber 706. The heating elements 710 and the temperature sensor(s) 711 are configured to maintain a certain temperature inside the sample chamber 706.

[0089] A shield 712 encircles the metal cage 708. The shield 712 is configured to provide additional magnetic field shielding or isolation for the sample chamber 706. The shield 712 can be comprised of lead or other magnetic shielding materials. The shield 712 is optional when sufficient shielding is provided by the sample chamber 706 and/or the metal cage 708.

[0090] Surrounding the shield 712 is a cryogen layer 716 with G10 insulation. The cryogen may be liquid helium. The cryogen layer 716 (also referred to as a cryogenic Dewar) is at an operating temperature of 4 degrees Kelvin. Surrounding the cryogen layer 716 is an outer shield 718. The outer shield 718 is comprised of nickel alloy and is configured to be a magnetic shield. The total amount of magnetic shielding provided by the detection unit 702 is approximately -100 dB, -100 dB, and -120 dB along the three orthogonal planes of a Cartesian coordinate system.

[0091] The various elements described above are electrically isolated from each other by air gaps or dielectric barriers (not shown). It should also be understood that the elements are not shown to scale relative to each other for ease of description.

[0092] A sample holder 720 can be manually or mechanically positioned within the sample chamber 706. The sample holder 720 may be lowered, raised, or removed from the top of the sample chamber 706. The sample holder 720 is

comprised of a material that will not introduce Eddy currents and exhibits little or no inherent molecular rotation. As an example, the sample holder 720 can be comprised of high quality glass or Pyrex.

[0093] The detection unit 702 is configured to handle solid, liquid, or gas samples. Various sample holders may be utilized in the detection unit 702. For example, depending on the size of the sample, a larger sample holder may be utilized. As another example, when the sample is reactive to air, the sample holder can be configured to encapsulate or form an airtight seal around the sample. In still another example, when the sample is in a gaseous state, the sample can be introduced inside the sample chamber 706 without the sample holder 720. For such samples, the sample chamber 706 is held at a vacuum. A vacuum seal 721 at the top of the sample chamber 706 aids in maintaining a vacuum and/or accommodating the sample holder 720.

[0094] A sense coil 722 and a sense coil 724, also referred to as detection coils, are provided above and below the sample holder 720, respectively. The coil windings of the sense coils 722, 724 are configured to operate in the direct current (DC) to approximately 50 kilohertz ( kHz) range, with a center frequency of 25 kHz and a self-resonant frequency of 8.8 MHz. The sense coils 722, 724 are in the second derivative form and are configured to achieve approximately 100% coupling. In one embodiment, the coils 722, 724 are generally rectangular in shape and are held in place by G10 fasteners. The coils 722, 724 function as a second derivative gradiometer.

[0095] Helmholtz coils 726 and 728 may be vertically positioned between the shield 712 and the metal cage 708, as explained herein. Each of the coils 726 and 728 may be raised or lowered independently of each other. The coils 726 and 728, also referred to as a white or Gaussian noise generation coils, are at room or ambient temperature. The noise generated by the coils 726, 728 is approximately 0.10 Gauss.

[0096] The degree of coupling between the emissions from the sample and the coils 722, 724 may be changed by repositioning the sample holder 720 relative to the coils 722, 724, or by repositioning one or both of the coils 726, 728 relative to the sample holder 720.

[0097] The processing unit 704 is electrically coupled to the coils 722, 724, 726, and 728. The processing unit 704 specifies the white or Gaussian noise to be

injected by the coils 726, 728 to the sample. The processing unit 104 also receives the induced voltage at the coils 722, 724 from the sample's electromagnetic emissions mixed with the injected Gaussian noise.

[0098] Referring to Figure 8, a processing unit employing aspects of the invention includes a sample tray 840 that permits a sample 842 to be inserted into, and removed from, a Faraday cage 844 and Helmholtz coil 746. A SQUID/gradiometer detector assembly 848 is positioned within a cryogenic dewar 850. A flux-locked loop 852 is coupled between the SQUID/gradiometer detector assembly 848 and a SQUID controller 854. The SQUID controller 854 may be a model iMC-303 iMAG multichannel controller provided by Tristan.

[0099] An analog noise generator 856 provides a noise signal (as noted above) to a phase lock loop 858. The x-axis output of the phase lock loop is provided to the Helmholtz coil 846, and may be attenuated, such as by 20 dB. The y-axis output of the phase lock loop is split by a signal splitter 860. One portion of the y-axis output is input the noise cancellation coil at the SQUID, which has a separate input for the gradiometer. The other portion of the y-axis signal is input oscilloscope 862, such as an analog/digital oscilloscope having Fourier functions like the Tektronix TDS 3000b (e.g., model 3032b). That is, the x-axis output of the phase lock loop drives the Helmholtz coil, and the y-axis output, which is in inverted form, is split to input the SQUID and the oscilloscope. Thus, the phase lock loop functions as a signal inverter. The oscilloscope trace is used to monitor the analog noise signal, for example, for determining when a sufficient level of noise for producing non-stationary spectral components is achieved. An analog tape recorder or recording device 864, coupled to the controller 854, records signals output from the device, and is preferably a wideband (e.g. 50 kHz) recorder. A PC controller 866 may be an MS Windows based PC interfacing with the controller 854 via, for example, an RS 232 port.

[00100] In Figure 9, a block diagram of another embodiment of the processing unit is shown. A dual phase lock-in amplifier 202 is configured to provide a first signal (e.g., "x" or noise signal) to the coils 726, 728 and a second signal (e.g., "y" or noise cancellation signal) to a noise cancellation coil of a superconducting quantum interference device (SQUID) 206. The amplifier 202 is configured to lock without an external reference and may be a Perkins Elmer model 7265 DSP lock-in amplifier. This amplifier works in a "virtual mode," where it locks to an initial reference

frequency, and then removes the reference frequency to allow it to run freely and lock to "noise."

[00101] An analog noise generator 200 is electrically coupled to the amplifier 202. The generator 200 is configured to generate or induce an analog white Gaussian noise at the coils 726, 728 via the amplifier 202. As an example, the generator 200 may be a model 1380 manufactured by General Radio.

[00102] An impedance transformer 204 is electrically coupled between the SQUID 206 and the amplifier 202. The impedance transformer 204 is configured to provide impedance matching between the SQUID 206 and amplifier 202.

[00103] The noise cancellation feature of the SQUID 206 can be turned on or off. When the noise cancellation feature is turned on, the SQUID 206 is capable of canceling or nullifying the injected noise component from the detected emissions. To provide the noise cancellation, the first signal to the coils 726, 728 is a noise signal at 20 dB or 35 dB above the molecular electromagnetic emissions sought to be detected. At this level, the injected noise takes on the characteristics of the molecular electromagnetic signal through stochastic resonance. The second signal to the SQUID 206 is a noise cancellation signal and is inverted from the first signal at an amplitude sufficient to null the noise at the SQUID output (e.g., 180 degrees out of phase with respect to the first signal).

[00104] The SQUID 206 is a low temperature direct element SQUID. As an example, the SQUID 206 may be a model LSQ/20 LTS dC SQUID manufactured by Tristan Technologies, Inc. Alternatively, a high temperature or alternating current SQUID can be used. The coils 722, 724 (e.g., gradiometer) and the SQUID 206 (collectively referred to as the SQUID/gradiometer detector assembly) combined has a magnetic field measuring sensitivity of approximately 5 microTesla/ $\sqrt{\text{Hz}}$ . The induced voltage in the coils 722, 724 is detected and amplified by the SQUID 206. The output of the SQUID 206 is a voltage approximately in the range of 0.2-0.8 microVolts.

[00105] The output of the SQUID 206 is the input to a SQUID controller 208. The SQUID controller 208 is configured to control the operational state of the SQUID 206 and further condition the detected signal. As an example, the SQUID controller 208 may be an iMC-303 iMAG multi-channel SQUID controller manufactured by Tristan Technologies, Inc.

[00106] The output of the SQUID controller 208 is inputted to an amplifier 210. The amplifier 210 is configured to provide a gain in the range of 0-100 dB. A gain of approximately 20 dB is provided when noise cancellation node is turned on at the SQUID 206. A gain of approximately 50 dB is provided when the SQUID 206 is providing no noise cancellation.

[00107] The amplified signal is inputted to a recorder or storage device 212. The recorder 212 is configured to convert the analog amplified signal to a digital signal and store the digital signal. In one embodiment, the recorder 212 stores 8600 data points per Hz and can handle 2.46 Mbits/sec. As an example, the recorder 212 may be a Sony digital audiotape (DAT) recorder. Using a DAT recorder, the raw signals or data sets can be sent to a third party for display or specific processing as desired.

[00108] A lowpass filter 214 filters the digitized data set from the recorder 212. The lowpass filter 214 is an analog filter and may be a Butterworth filter. The cutoff frequency is at approximately 50 kHz.

[00109] A bandpass filter 216 next filters the filtered data sets. The bandpass filter 216 is configured to be a digital filter with a bandwidth between DC to 50 kHz. The bandpass filter 216 can be adjusted for different bandwidths.

[00110] The output of the bandpass filter 216 is the input to a Fourier transformer processor 218. The Fourier transform processor 218 is configured to convert the data set, which is in the time domain, to a data set in the frequency domain. The Fourier transform processor 218 performs a Fast Fourier Transform (FFT) type of transform.

[00111] The Fourier transformed data sets are the input to a correlation and comparison processor 220. The output of the recorder 212 is also an input to the processor 220. The processor 220 is configured to correlate the data set with previously recorded data sets, determine thresholds, and perform noise cancellation (when no noise cancellation is provided by the SQUID 206). The output of the processor 220 is a final data set representative of the spectrum of the sample's molecular low frequency electromagnetic emissions.

[00112] A user interface (UI) 222, such as a graphical user interface (GUI), may also be connected to at least the filter 216 and the processor 220 to specify signal processing parameters. The filter 216, processor 218, and the processor 220 can be implemented as hardware, software, or firmware. For example, the filter 216

and the processor 218 may be implemented in one or more semiconductor chips. The processor 220 may be software implemented in a computing device.

[00113] This amplifier works in a "virtual mode," where it locks to an initial reference frequency, and then removes the reference frequency to allow it to run freely and lock to "noise." The analog noise generator (which is produced by General Radio, a truly analog noise generator) requires 20 dB and 45-dB attenuation for the Helmholtz and noise cancellation coil, respectively.

[00114] The Helmholtz coil may have a sweet spot of about one cubic inch with a balance of 1/100<sup>th</sup> of a percent. In an alternative embodiments, the Helmholtz coil may move both vertically, rotationally (about the vertical access), and from a parallel to spread apart in a pie shape. In one embodiment, the SQUID, gradiometer, and driving transformer (controller) have values of 1.8, 1.5 and 0.3 micro-Henrys, respectively. The Helmholtz coil may have a sensitivity of 0.5 Gauss per amp at the sweet spot.

[00115] Approximately 10 to 15 microvolts may be needed for a stochastic response. By injecting noise, the system has raised the sensitivity of the SQUID device. The SQUID device had a sensitivity of about 5 femtotesla without the noise. This system has been able to improve the sensitivity by 25 to 35 dB by injecting noise and using this stochastic resonance response, which amounts to nearly a 1,500% increase.

[00116] After receiving and recording signals from the system, a computer, such as a mainframe computer, supercomputer or high-performance computer does both pre and post processing, such by employing the Autosignal software product by Systat Software of Richmond CA, for the pre-processing, while Flexpro software product does the post-processing. Flexpro is a data (statistical) analysis software supplied by Dewetron, Inc. The following equations or options may be used in the Autosignal and Flexpro products.

Forward Transform 
$$X_n = \sum_{k=0}^{N-1} x_k e^{-\frac{i2\pi kn}{N}}$$

Reverse Transform 
$$X_k = 1/N \sum_{n=0}^{N-1} X_n e^{\frac{-i2\pi kn}{N}}$$

FFT Algorithm:

Best Exact N using Temperton's Prime Factor FFT (C. Temperton, "Implementation of a Self-Sorting In-Place Prime Factor FFT Algorithm, Journal of Computation Physics, v. 58, p. 283, 1985).

Data Tapering Windows:

[cs4 BHarris min]  $0.35875 - 0.48829 \cos(2\pi i/(n-1)) + 0.14128 \cos(4\pi i/(n-1)) - 0.01168 \cos(6\pi i/(n-1))$ ,  $i=0..n-1$

[Rectangular] No fixed shape tapering available (Oscilloscope)

Magnitude:  $\sqrt{\text{Re} \cdot \text{Re} + \text{Im} \cdot \text{Im}}$  [Re = real component, Im = imaginary component]

Amplitude:  $2.0 \cdot \sqrt{\text{Re} \cdot \text{Re} + \text{Im} \cdot \text{Im}} / n$

db, decibels:  $10.0 \cdot \log_{10}(\text{Re} \cdot \text{Re} + \text{Im} \cdot \text{Im})$

Averaging Replicates:

[00117] Replicates are based on the X-values coinciding to within 1e-8 fractional precision.

Reference Subtraction:

[00118] Reference Signal Subtraction (baseline noise) is performed on Y axis (amplitude) at each point (channel) along the X (time) axis. Negative Y values are then zeroed.

Cross-Correlation:

[00119] The function calculates the cross correlation function using summation and integration. Since the signal is transient, the correlation function is calculated using direct multiplication and integration. All of the values required for the calculation which lie outside the source channels (data series) are taken to be 0. The points for which  $t < 0$  are also calculated.

Fourier Significance Levels:

[00120] Monte Carlo data is fitted to parametric models. Where data size N is the only factor, univariate TableCurve 2D parametric models are used. For a segmented FFT where segment size and overlap are additional influences, trivariate Chebyshev polynomials are implemented. These are options selected under

Autosignal. One could have data sets that analyze individually, or could be analyzed in an overlapping fashion where data set one would be analyzed, then the second half of data set one and the first half of data set two, then data set two, then the second half.

[00121] A flow diagram of the signal detection and processing performed by the system 100 is shown in Figure 10. When a sample is of interest, at least four signal detections or data runs are performed: a first data run at a time  $t_1$  without the sample, a second data run at a time  $t_2$  with the sample, a third data run at a time  $t_3$  with the sample, and a fourth data run at a time  $t_4$  without the sample. Performing and collecting data sets from more than one data run increases accuracy of the final (e.g., correlated) data set. In the four data runs, the parameters and conditions of the system 100 are held constant (e.g., temperature, amount of amplification, position of the coils, the noise signal, etc.).

[00122] At a block 300, the appropriate sample (or if it's a first or fourth data run, no sample), is placed in the system 100. A given sample, without injected noise, emits electromagnetic emissions in the DC-50 kHz range at an amplitude equal to or less than approximately 0.001 microTesla. To capture such low emissions, a white Gaussian noise is injected at a block 301.

[00123] At a block 302, the coils 722, 724 detect the induced voltage representative of the sample's emission and the injected noise. The induced voltage comprises a continuous stream of voltage values (amplitude and phase) as a function of time for the duration of a data run. A data run can be 2-20 minutes in length and hence, the data set corresponding to the data run comprises 2-20 minutes of voltage values as a function of time.

[00124] At a block 304, the injected noise is cancelled as the induced voltage is being detected. This block is omitted when the noise cancellation feature of the SQUID 206 is turned off.

[00125] At a block 306, the voltage values of the data set are amplified by 20-50 dB, depending on whether noise cancellation occurred at the block 304. And at a block 308, the amplified data set undergoes analog to digital (A/D) conversion and is stored in the recorder 212. A digitized data set can comprise millions of rows of data.

[00126] After the acquired data set is stored, at a block 310 a check is performed to see whether at least four data runs for the sample have occurred (e.g.,

have acquired at least four data sets). If four data sets for a given sample have been obtained, then lowpass filtering occurs at a block 312. Otherwise, the next data run is initiated (return to the block 300).

[00127] After lowpass filtering (block 312) and bandpass filtering (at a block 314) the digitized data sets, the data sets are converted to the frequency domain at a Fourier transform block 316.

[00128] Next, at a block 318, like data sets are correlated with each other at each data point. For example, the first data set corresponding to the first data run (e.g., a baseline or ambient noise data run) and the fourth data set corresponding to the fourth data run (e.g., another noise data run) are correlated to each other. IF the amplitude value of the first data set at a given frequency is the same as the amplitude value of the fourth data set at that given frequency, then the correlation value or number for that given frequency would be 1.0. Alternatively, the range of correlation values may be set at between 0-100. Such correlation or comparison also occurs for the second and third data runs (e.g., the sample data runs). Because the acquired data sets are stored, they can be accessed at a later time as the remaining data runs are completed.

[00129] When the SQUID 206 provides no noise cancellation, then predetermined threshold levels are applied to each correlated data set to eliminate statistically irrelevant correlation values. A variety of threshold values may be used, depending on the length of the data runs (the longer the data runs, greater the accuracy of the acquired data) and the likely similarity of the sample's actual emission spectrum to other types of samples. In addition to the threshold levels, the correlations are averaged. Use of thresholds and averaging correlation results in the injected noise component becoming very small in the resulting correlated data set.

[00130] If noise cancellation is provided at the SQUID 206, then the use of thresholds and averaging correlations are not necessary.

[00131] Once the two sample data sets have been refined to a correlated sample data set and the two noise data sets have been refined to a correlated noise data set, the correlated noise data set is subtracted from the correlated sample data set. The resulting data set is the final data set (e.g., a data set representative of the emission spectrum of the sample) (block 320).

[00132] Since there can be 8600 data points per Hz and the final data set can have data points for a frequency range of DC-50 kHz, the final data set can comprise

several hundred million rows of data. Each row of data can include the frequency, amplitude, phase, and a correlation value.

[00133] In Figures 11A and 11B, there are shown examples of sample emission spectrums. A Fourier plot 400 shown in Figure 11A corresponds to a spectrum of a sample of saturated sodium chloride solution. A Fourier plot 500 shown in Figure 11B corresponds to a spectrum of a sample of an enzyme.

[00134] Referring to Figure 16, another alternative embodiment to the systems described above will now be described as a system 1600. In general, alternatives and alternative embodiments described herein are substantially similar to previously described embodiments, and the same reference numbers often identify common elements and functions. Only significant differences in construction or operation are described in detail.

[00135] A second derivative gradiometer is shown as 1602, where the target sample is positioned between upper and lower pairs of coils. Two inner coils on opposite sides of the sample complement each other, while two outer coils (top and bottom coils) each complement each other, and oppose the two inner coils. Such an arrangement allows for greater signal extraction from the sample and improved noise rejection.

[00136] While shown in the Figures and described in greater detail below, the system 1600 employs a concentric series of elements and an arrangement along a central axis extending into the dewar. A stepper motor 1604 allows the sample to be positioned axially within this arrangement of concentric elements. In particular, the sample may be positioned at a desired location within a middle of the gradiometer 1602.

[00137] Likewise, a micrometer adjustment mechanism 1606, such as a mechanical micrometer or stepper motor, allows the Helmholtz coils to be aligned with respect to elements in the system (such as the sample and gradiometer). Such an adjustment of the Helmholtz coil aids in manufacture and calibration of the system 1600, as well as allowing precise alignment of fields within the system, such as providing a uniform field with respect to the gradiometer 1602. It may be useful to also provide a field off set or change in field gradient to produce a better stochastic result, to offset noise in the system, or to provide other benefits.

[00138] Figures 17A, 17B, and 18 show more clearly the concentric arrangement of elements within the system 1600, wherein the sample tube extends

axially through a center of a low pass filtering metal shield 1802 (such as a stainless steel alloy) to pass signals below 2 kHz. An outer magnetic (MU) shield surrounds the gradiometer, Helmholtz coils and sample. The arrangement of system 1600 is generally self-explanatory with respect to the Figures.

[00139] The random white noise generator, model 1381, manufactured by General Radio and described above, may be replaced by a programmable Gaussian white noise generator manufactured by Noise/Com. Such a generator employs two outputs, one inverted from the other. One output may be connected to the Helmholtz coil, with the other (inverted) output connected to the SQUID noise cancellation coil noted above.

[00140] Likewise, as shown in Figure 19, the Tektronix digital oscilloscope noted above may be replaced by a two-channelled dynamic signal analyzer 1902, model SR 785, manufactured by Stanford Research Systems. Such a signal analyzer may process incoming signals by sampling multiple time domain signals and averaging them across multiple frequency domain FFT's. This may result in a full spectrum frequency domain record of all non-random signal components. Other changes that may be made include replacing the digital audio tape storage system with a digital versatile disk (DVD) recorder 1904. Further, a data acquisition board 1906 manufactured by Keithley, model 3801, may be used, which works with software for generating histograms, as described below.

[00141] In the alternative embodiment shown in Figure 19, a noise cancellation coil 1908 is connected between the gradiometer and SQUID. (While a first derivative gradiometer is shown, a second derivative gradiometer, such as that shown in Figure 16, may be used.) While not shown in Figure 19, an inverted noise channel (inverted with respect to noise applied to the Helmholtz coils) may be applied to the noise cancellation coil 1908 (and may first pass through an impedance transformer that attenuates the noise signal by, for example, 45 dB). In an alternative embodiment, not shown, the noise cancellation coil may be positioned within the SQUID 120, between the SQUID input and output coils.

[00142] Referring to Figures 24-27, alternative embodiments to the systems described above are presented. Referring to Figure 24, a noise source 2402 provides noise input to a detector system 2400. It may provide stationary white Gaussian noise, which is random Gaussian noise that has no predictable future components. Alternatively, the noise source 2402 may provide structured noise,

which is noise that contains a logarithmic characteristic that shifts energy from one region of the spectrum to another, or provides a random time element while the amplitude remains constant (e.g. pulses of varying width, but of substantially constant amplitude). These two represent pink and uniform noise, respectively, as compared to truly random noise which has no predictable future component. Further, the noise source may produce uniform noise, which is noise having a constant amplitude, but which changes in time, frequency or both.

[00143] The noise source 2402 is a two-channel noise generator that delivers noise to the Helmholtz coils 726 and 728, and delivers an inverted version of the noise to the noise coil 1908. As shown, the noise coil 1908 is actually a pair of noise coils forming a transformer to inductively couple the two coils. Of course, other coils or methods of applying the inverted noise to the input of the SQUID 206 may be employed, as those skilled in the art will recognize. The inverted version of the noise cancels remnants of the non-inverted noise detected by the second derivative gradiometer 1602.

[00144] Referring to Figure 25, an alternative embodiment to the system 2400 is shown as a detector system 2500. Here, the noise source 2402 is paired with a second, independent noise source 2502. The first noise source 2402 operates as it does in the system 2400. This noise source takes advantage of molecular oscillation in raising a sub-threshold molecular signal to detectable levels using principles of stochastic resonance. The second noise source 2502, which can be substantially similar to the first noise source, provides a non-inverted noise signal to a second noise coil 2504 positioned between the noise coil 1908 and the input of the SQUID 206. An inverted version of the noise is then applied to the output of the SQUID 206 via a noise coil (or transformer) 2506. The second noise source 2502 employs the noise at the input of the SQUID and cancels that noise at the SQUID's output.

[00145] The noise cancellation model of the system 2500 takes advantage of the SQUID's ability to act as a bi-stable oscillator combining a sub-threshold molecular signal with noise, thereby raising the sub-threshold signal to detectable levels via stochastic resonance. The system 2500 affectively provides two stages of stochastic amplification. Further, the system 2500 allows the user to independently improve the signal to noise ratio at the gradiometer and at the SQUID. While the noise sources may be substantially similar, different noise sources may be employed depending upon the application.

[00146] Referring to Figure 26, another alternative embodiment to the systems 2400 and 2500 is shown as a system 2600. Unlike the system 2400, the system 2600 applies the inverted version of the noise at the output to the SQUID 206. Thus, the inverted copy of the noise is delivered to the noise cancellation coil 1908 as located between the SQUID 206 and the flux lock loop or other signal processing element (not shown). (This embodiment requires correction for changes in phase, which may be handled by the flux lock loop, by a lock-in amplifier, and so forth.) The system 2600 again takes advantage of the SQUID's ability to act as a bi-stable oscillator combining the noise emitted by the Helmholtz coils 726, 728 with a sub-threshold molecular signal using stochastic resonance to raise the sub-threshold molecular signal to detectable levels.

[00147] Referring to Figure 27, a system 2700 employs a random number generator or other software-based system to generate stochastic amplification at the output of the SQUID 206. Here, a random number generator or other suitable software-based system injects engineered noise 2701 to the Helmholtz coils 726, 728. This engineered noise is a sequential set of random numbers that may be stored in Excel format. These random numbers are used to drive the production of noise useful in raising a sub-threshold signal to detectable levels by means of stochastic resonance.

[00148] The output of the SQUID 206 is recorded by the data recorder 212. A signal processor 2704 (which may be software running on a computer, one or more DSPs, etc.) subtracts the engineered noise from the recorded data signal. In other words, the random numbers represented in the Excel format are extracted from the SQUID output by post-processing in such a way that the random numbers are subtracted from the SQUID output. The stochastic amplification occurs all in software, using the output from the SQUID. Through the use of software and signal processing, uniform noise is generated where the amplitude of the noise is uniform, but its frequency is random. An example of a software package capable of generating the random number signal (and then removing it) is Mathcad® by Mathsoft.

[00149] Timing marks, such as elevated amplitudes at regular intervals, may be included in the sequence of random numbers as an aid in aligning the noise input signal with the SQUID output signal. By aligning these markers between the input and output signals permits the noise to be readily subtracted out. The result is a

signal product 2706 that includes only the molecular signal with the engineered noise subtracted therefrom.

### III. Histogram Method of Generating Spectral Information

[00150] Figure 20 is a high level data flow diagram in the histogram method for generating spectral information. Data acquired from the SQUID (box 2002) or stored data (box 2004) is saved as 16 bit WAV data (box 2006), and converted into double-precision floating point data (box 2008). The converted data may be saved (box 2010) or displayed as a raw waveform (box 2012). The converted data is then passed to the algorithm described below with respect to Figure 21, and indicated by the box 2014 labeled Fourier Analysis. The histogram can be displayed at 2016.

[00151] With reference to Figure 21, the general flow of the histogram algorithm is to take a discrete sampled time-domain signal and use Fourier analysis to convert it to a frequency domain spectrum for further analysis. The time-domain signals are acquired from an ADC (analog/digital converter) and stored in the buffer indicated at 2102. This sample is *SampleDuration* seconds long, and is sampled at *SampleRate* samples per second, thus providing *SampleCount* (*SampleDuration* \* *SampleRate*) samples. The *FrequencyRange* that can be recovered from the signal is defined as half the *SampleRate*, as defined by Nyquist. Thus, if a time-series signal is sampled at 10,000 samples per second, the *FrequencyRange* will be 0 Hz to 5 kHz. One Fourier algorithm that may be used is a Radix 2 Real Fast Fourier Transform (RFFT), which has a selectable frequency domain resolution (*FFTSize*) of powers of two up to  $2^{16}$ . An *FFTSize* of 8192 is selected, to provide provides enough resolution to have at least one spectrum bin per Hertz as long as the *FrequencyRange* stays at or below 8 kHz. The *SampleDuration* should be long enough such that  $SampleCount > (2 * FFTSize * 10)$  to ensure reliable results.

[00152] Since this FFT can only act on *FFTSize* samples at a time, the program must perform the FFT on the samples sequentially and average the results together to get the final spectrum. If one chooses to skip *FFTSize* samples for each FFT, a statistical error of  $1 / FFTSize^{0.5}$  is introduced. If, however, one chooses to overlap the FFT input by half the *FFTSize*, this error is reduced to  $1 / (0.81 * 2 * FFTSize)^{0.5}$ . This reduces the error from 0.0110485435 to 0.0086805556. Additional information about errors and correlation analyses in general, consult Bendat & Piersol, "Engineering Applications of Correlation and Spectral Analysis", 1993.

[00153] Prior to performing the FFT on a given window, a data tapering filter may be applied to avoid spectral leakage due to sampling aliasing. This filter can be chosen from among: Rectangular (no filter), Hamming, Hanning, Bartlett, Blackman and Blackman/Harris, as examples.

[00154] In an exemplary method, and as shown in box 2104, we have chosen 8192 for the variable FFTSize, which will be the number of time-domain samples we operate on at a time, as well as the number of discrete frequencies output by the FFT. Note that FFTSize = 8192 is the resolution, or number of bins in the range which is dictated by the sampling rate. The variable n, which dictates how many discrete RFFT's (Real FFT's) performed, is set by dividing the SampleCount by FFTSize \* 2, the number of FFT bins. In order for the algorithm to generate sensible results, this number n should be at least 10 to 20 (although other values are possible), where more may be preferred to pick up weaker signals. This implies that for a given SampleRate and FFTSize, the SampleDuration must be long enough. A counter m, which counts from 0 to n, is initialized to zero, also as shown in box 2104.

[00155] The program first establishes three buffers: buffer 2108 for FFTSize histogram bins, that will accumulate counts at each bin frequency; buffer 2110 for average power at each bin frequency, and a buffer 2112 containing the FFTSize copied samples for each m.

[00156] The program initializes the histograms and arrays (box 2113) and copies FFTSize samples of the wave data into buffer 2112, at 2114, and performs an RFFT on the wave data (box 2115). The FFT is normalized so that the highest amplitude is 1 (box 2116) and the average power for all FFTSize bins is determined from the normalized signal (box 2117). For each bin frequency, the normalized value from the FFT at that frequency is added to each bin in buffer 2108 (box 2118).

[00157] In box 2119 the program then looks at the power at each bin frequency, relative to the average power calculated from above. If the power is within a certain factor epsilon (between 0 and 1) of the average power, then it is counted and the corresponding bin is incremented in the histogram buffer at 16. Otherwise it is discarded.

[00158] Note that the average power it is comparing to is for this FFT instance only. An enhanced, albeit slower algorithm might take two passes through the data and compute the average over all time before setting histogram levels. The comparison to epsilon helps to represent a power value that is significant enough for

a frequency bin. Or in broader terms, the equation employing epsilon helps answer the question, "is there a signal at this frequency at this time?" If the answer is yes, it could be one of two things: (1) stationary noise which is landing in this bin just this one time, or (2) a real low level periodic signal which will occur nearly every time. Thus, the histogram counts will weed out the noise hits, and enhance the low level signal hits. So, the averaging and epsilon factor allow one to select the smallest power level considered significant.

[00159] Counter *m* is incremented at box 2120, and the above process is repeated for each *n* set of WAV data until *m* is equal to *n* (box 2121). At each cycle, the average power for each bin is added to the associated bin at 2118, and each histogram bin is incremented by one when the power amplitude condition at 2114 is met.

[00160] When all *n* cycles of data have been considered, the average power in each bin is determined by dividing the total accumulated average power in each bin by *n*, the total number of cycles (box 2122) and the results displayed (box 2123). Except where structured noise exists, e.g., DC = 0 or at multiples of 60 Hz, the average power in each bin will be some relatively low number. This is indicated in the plots shown at Figures 22A-D (the histograms generated at 400, 600, 700, and 900 mV). The plots of Figures 22A-22D show only a portion of the histogram bins, namely a spectrum from 7953Hz through 8533Hz. As shown in Figures 22A and 22B, no stochastic event is visible at 400 mV or 600 mV of injected noise, respectively. However, as shown in Figure 22C, at 700 mV, a visible stochastic event is evident. Thereafter, as shown in Figure 22D, at 900 mV, the stochastic event is lost.

[00161] The histogram produced by the above steps contains, in each bin, a count between 0 and *n* of the number of times that the power at that frequency was above ( $\epsilon \times$  the average power for that whole FFT output). If a bin count is incremented due to unstructured noise, that noise will be distributed across all the frequency bins over time, thus not adding up to much in a given bin. If there is consistent signal at a given frequency, it will be present at each of the *n* time slices and thus have a bin count approaching *n*. Large amplitude noise, such as sixty hertz and its harmonics have both high bin counts as well as high average power. We can differentiate between these frequencies, and the ones we are interested in that have low average power, but high bin counts.

[00162] Figures 22A-22D show histograms generated by the method at four different noise power inputs. As shown, the program may display average power at each frequency as a vertical bar. The histogram bin counts may be represented as a connected upper line. If the power is considered "low" (e.g. less than average/3), and the histogram has a certain count, then a connecting line may become observable between the peak of a power bar and a peak of a histogram bar. Bins highlighted by the connecting lines are likely candidates for low energy molecular spectra.

[00163] It can be appreciated from Figures 22A-22D and from the above, that there are two settings of note used in generating a meaningful histogram, that is, a histogram that shows stochastic resonance effects related to a sample being interrogated. The first is the power level of Gaussian white noise supplied to the sample. If this level is too low, the noise level is not sufficient to create stochastic resonance and the bin histogram reflects noise only. If the power input is too high, the average power level calculated for each bin is high and stochastic events cannot be distinguished.

[00164] The second setting is the value of epsilon. This value determines a power value that will be used to distinguish an event over average value. At a value of 1, no events will be detected, since power will never be greater than average power. As epsilon approaches zero, virtually every value will be placed in a bin. Between 0 and 1, and typically at a value that gives a number of bin counts between about 20-50% of total bin counts for structured noise, epsilon will have a maximum "spectral character," meaning the stochastic resonance events will be most highly favored over pure noise.

[00165] Therefore, in practicing the invention, one can systematically increase the power gain on the noise input, e.g., in 100 mV increments between 0 and 1 V, and at each power setting, adjust epsilon until a histogram having well defined peaks is observed. Where, for example, the sample being processed represents a 20 second time interval, total processing time for each different power and epsilon will be about 25 seconds. When a well-defined signal is observed, either the power setting or epsilon or both can be refined until an optimal histogram, meaning one with the largest number of identifiable peaks, is produced.

[00166] Under this algorithm, numerous bins may be filled and associated histogram rendered for low frequencies due to the general occurrence of noise (such

as environmental noise) at the low frequencies. Thus, the system may simply ignore bins below a given frequency (e.g., below 1 kHz), but still render sufficient bin values at higher frequencies to determine unique signal signatures between samples.

[00167] Alternatively, since a purpose of the epsilon variable is to accommodate different average power levels determined in each cycle, the program could itself automatically adjust epsilon using a predefined function relating average power level to an optimal value of epsilon.

[00168] Similarly, the program could compare peak heights at each power setting, and automatically adjust the noise power setting until optimal peak heights or character is observed in the histograms.

[00169] Although the value of epsilon may be a fixed value for all frequencies, it is also contemplated to employ a frequency-dependent value for epsilon, to adjust for the higher value average energies that may be observed at low frequencies, e.g., DC to 1,000. A frequency-dependent epsilon factor could be determined, for example, by averaging a large number of low-frequency FFT regions, and determining a value of epsilon that "adjusts" average values to values comparable to those observed at higher frequencies.

[00170] Referring to Figures 23A-23C, an example of a user interface for generating histograms is shown. A slider bar 2302 determines the length of a sample waveform segment, such as up to 300-600 seconds, and allows a user to effectively scroll within a waveform. A box 2304 allows the user to set a Nyquist frequency, such as 5, 10 or 20 kHz, and also provided is an adjacent reset button. A slider bar 2306 allows the user to move the baseline for histograms, while a 60Hz checkbox 2308 allows the user to identify the 60Hz bin and all related 60Hz harmonics with vertical lines (as shown in Figure 23C). When an acquire button 2312 is selected, the software generates or acquires a waveform from a sample, such as that shown in Figure 23B. When an fft button 2310 is selected, the software generates a histogram plot, such as that shown in Figure 23C.

#### IV. Methods and Applications

[00171] This section describes the use of the apparatus described above for interrogating a sample, and a variety of applications of the apparatus in characterizing a sample and in detecting sample components. Also disclosed, in

accordance with the invention, is a low-frequency spectroscopic signature or data set by which a sample can be characterized, and a time-domain signal of a sample, used, for example, in generating the sample spectroscopic signature.

A. Method of interrogating a sample

[00172] An objective of the method of the invention is to generate spectroscopic information relating a sample being interrogated. As will be seen, the information may be in the form of a spectral plot, in a selected low-frequency spectral range, or a data set which identifies low-frequency spectral components characterizing the sample, or actual identification of a sample or sample components, based on the characteristic frequencies identified for the sample.

[00173] The sample may be any material having atomic or molecular components, e.g., ionic salt components or molecular compound in ionized or nonionized form, or protonated or non-protonated form, that has molecular rotation, and preferably a dipole moment such that molecular rotation in a magnetic field, e.g., the earth's magnetic field, is effective to produce a low-frequency electromagnetic emission. The sample is typically a liquid sample, but may be gaseous or solid or semi-solid as well, as long as at least one component of the sample has one or more rotational degrees of freedom. Typical samples are aqueous or organic solutions having one or more solute components, which may be the sample material of interest, dissolved in the solvent.

[00174] The sample is placed in a suitable vessel, preferably one such as Pyrex glass that has little observable low-frequency spectral components, and the vessel is then positioned in the apparatus container as described in Section II. With the sample positioned in the apparatus container, the Gaussian noise generator is activated to inject Gaussian noise into the sample. The amplitude (mean amplitude) of Gaussian noise injected is preferably sufficient to produce non-stationary composite time-domain signal components. This may be done, for example, using an oscilloscope with a Fourier transform capability, and observing the frequency-domain signal in a suitable range, e.g., 200-800Hz window. A suitable noise level is selected when detectable frequency components are first observed.

[00175] During noise injection, the recording device records a time-domain electromagnetic signal from the detector over a preset time interval. The recording interval may be relatively short, e.g., 30-60 seconds, or may be several minutes or

more, depending on the final spectral resolution required. The signals recorded are stored in a suitable signal storage device, e.g., a tape or hard disc, for use in later signal processing operations now to be described.

[00176] In general, it is desirable to enhance sample signal components by cross-correlating the sample time-domain signal recorded with a second time-domain signal of the same sample or, less preferably, an identical sample or a sample having the same sample components of interest. The recording time for the second signal is preferably the same as for the first signal. The two signals are cross-correlated using a standard cross-correlation algorithm in the time domain. This results in a spreadsheet or spectrum identifying the signal spectral components that are common in both signals that hold up over time, and a correlation value for each component which measures the relationship between spectral components common to both signals.

[00177] The improvement in spectral resolution obtained by the signal cross-correlation is seen in the Figures 12A and 12B, and Figures 13A and 13B. The Figures are Fast Fourier transforms of a first time-dependent signal in the frequency domain (Figures 12A and 13A) or a fast Fourier transform of the first and second cross-correlated frequency-domain spectra (the spreadsheet referred to above) (Figures 13B and 13B) to plot the spectral components in the frequency domain, and in the spectral range of 500-530 Hz.

[00178] Comparing Figures 12A and 12B for a NaCl sample, it is seen that the cross-correlation signal processing significantly enhances signal-to-noise ratio, brings out much more detail in the sample-specific spectral component whose peak is at 522.5 Hz, and also produces a significantly refined peak position. Similar (and exemplary) results were observed for the alkyl ether sulfate sample, whose spectral features in the 500-530 Hz range are seen in Figures 13A and 13B for uncorrelated and correlated signals, respectively. As with the NaCl sample, the spectrum derived from the correlated signals gave much lower signal-to-noise ratio, much more detail and information as to sample-specific spectral components. The signal correlation can also be applied, conventionally, to produce a spreadsheet relating frequency and phase (rather than frequency and amplitude).

[00179] The correlated time-domain spectrum from above is plotted in the frequency domain by applying a fast Fourier transform to the spectrum, where the spectral correlations values are represented in the y axis as amplitudes. The plot is

within the frequency range DC to 50 kHz, preferably in the region DC to 6.5 kHz. As will be seen below, the dominant spectral features of many samples are found in the 100-1,500 Hz range, particularly the 500-550 Hz range; and thus the spectrum generated may be confined accordingly, e.g., in the 500-530 Hz range. The FTT is carried out by a well known FTT algorithm. The correlated time-domain signal may also, or alternatively, be transformed to phase-domain or amplitude or magnitude domain signals, to extract signal information related to phase or amplitude components of the sample spectrum.

[00180] Once the frequency-domain spectrum is generated, either by the cross-correlating or FFT step, the spectrum is used to identify one or more low-frequency signal components that are characteristic of the sample being interrogated. This step may be performed by the user from direct viewing or by computer analysis of the spectra.

[00181] Figures 14A-14F show spectral features for the samples deionized water (Figure 14A), saturated NaCl (Figure 14B), 1% NaCl in deionized water (Figure 14C), saturated NaBr (Figure 14D), alkyl ether sulfate (Figure 14E), and empty sample vessel (Figure 14F), all in the spectral range of about 500-530. As seen, each sample has distinctive spectral components characterized by one or more peaks at well defined frequencies.

#### B. Characterizing a sample

[00182] Accordance with another aspect of the invention, the method above is used to generate a data set of low-frequency spectral components of a given sample, also referred to herein as a low-frequency signature signal of the material.

[00183] The 500-530 spectral range shown for the several samples above was selected to illustrate having prominent spectral features in the various samples. In order to obtain a more complete data set of spectral frequency components of a sample, spectral components over a wider frequency range, e.g., 100-1,500 Hz, should be determined. In one aspect, the invention includes a data set of spectral components associated with a given sample material, e.g., a solvent, gas, or solute component of a solution. The data set includes a list of the low-frequency spectral components of the sample, e.g., in the 100-1,500 Hz range, whose cross-spectral correlations have a selected statistical measure above background spectral noise, or selected ones of these components that are unique to the sample.

[00184] A variety of signal-analysis methods may be employed in generating the low-frequency data set for a given sample. In one exemplary method, a cross-correlated sample signal spectrum is compared with a cross-correlated noise (no sample) signal. The algorithm next advances incremental, e.g., in 0.1 Hz intervals across the cross-correlated sample spectrum and the cross-correlated noise spectrum, looking at the correlation value at each frequency point, and subtracts the noise correlation from the sample correlation at that point, to yield a frequency plot of corrected correlation values. These values will be relative to a particular sample, and depend, for example, on the relative amplitude of any noise component.

[00185] In general, frequency components having a higher correlation value (relative to the other values in that sample) will tend to hold up (be observed) over many interrogations of the same sample. To identify those that do hold up, the frequency components observed for the sample over two or more sample sets, each obtained as above, are compared, and only those that are seen in two (or more, if available) sets are taken as valid components of the data set for that sample. In the tables below, data sets for several samples (as identified in the tables) are given along with the correlations determined from a single sample interrogation. Those values indicated in italics (typically having the smaller correlation values) were found not to hold up in multiple data sets from the same sample material.

[00186] Thus, for example, for the saturated NaCl sample in Table 1, spectral components at 522.58, 523.12, 523.47, and 523.85 Hz correlate from sample to sample, and would form a data set for the sample in the frequency range 500-530 Hz. Additional members of the data set may be included in an expanded frequency range.

[00187] Similarly, for the amino acid sample of Table 3, the data set would include components at 262.93, 257.81, 257.23, 536.68, 448.05, 531.37, 528.80, 593.44, 588.68, 583.74, 578.61, 769.59, and 744.14 in the frequency range of between about 250 and 1,400 Hz. The greater spectral composition of the amino acid sample, relative to NaCl, presumably reflects in part, the greater complexity of the sample molecule.

Reversing Noise →	NaCl (Sat)		NaCl (1%)		NaBr (Sat)	
	Frequency / Correlation		Frequency / Correlation		Frequency / Correlation	
	√	A	√	A	√	A
	522.58	.3762	521.12	1.4161	520.57	2.0847
	523.12	.1732	521.48	1.4100	519.84	2.0704
	523.47	.1235	515.99	1.3865	509.37	2.0304
	523.85	.1021	520.75	1.3641	513.45	2.0155
	507.38	.0832	514.34	1.3735	516.35	1.9950
	524.43	.0768	525.86	1.3440	519.46	1.9950
	512.71	.0753	523.70	1.3400	518.33	1.9929
	—	—	526.61	1.3364	522.78	1.9635

Reversing Noise →	DI Water		Alkyl Ether Sulfate		Noise	
	Frequency / Correlation		Frequency / Correlation		Frequency / Correlation	
	√	A	√	A	√	A
	521.12	1.5324	517.81	.3376	514.34	.0734
	521.67	1.0818	516.50	.3375	513.79	.0432
	520.20	1.0630	517.08	.2776	506.28	.0326
	511.23	1.0502	515.46	.2749	512.70	.0277
	515.44	1.0457	518.37	.2508	522.58	.0220
	513.06	1.0451	519.47	.2425	525.15	.0177
	525.51	1.0371	515.44	.2400	516.36	.0149
	520.75	1.0301	519.84	.2383	523.13	.0140

Spectra Number	Frequency (Hz)	Correlation Factor
1	262.93	.139
2	340.39	.134
3	257.81	.126
4	357.23	.114
5	417.48	.110
6	536.68	.101
7	448.05	.096

Spectra Number	Frequency (Hz)	Correlation Factor
8	531.37	.096
9	528.80	.077
10	593.44	.071
11	588.68	.065
12	583.74	.058
13	1408.99	.052
14	840.08	.050
15	1393.99	.048
16	578.61	.045
17	1348.99	.044
18	769.59	.042
19	1042.96	.042
20	1238.52	.042
21	1472.16	.042
22	1062.92	.041
23	1281.73	.041
24	744.14	.039

[00188] The data above demonstrates that both simple and more complex molecular samples can be characterized in terms of unique low-frequency spectral components. The data set associated with a given sample material may also include (as shown in the tables) the associated correlations values of the spectral components. The data set may be used for example, in identifying components in an unknown sample and/or for estimating the relative concentrations of a material in a sample. The use of the method for identifying low-concentration components in a sample is discussed in the next section.

#### C. Identifying components in a sample

[00189] It is often desirable to detect sample components, e.g., trace contaminants, present in a multi-component sample material, such as a liquid sample with unknown contaminants, or other samples capable of holding or supporting a contaminant that it is desired to detect.

[00190] An analytical method for detecting a component of a sample, in accordance with another aspect of the invention, includes first identifying the low-

frequency sample spectral components of a sample (i) in a selected frequency range between DC and 50 kHz (ii) whose cross-spectral correlations have a selected statistical measure above background spectral noise, as described above.

[00191] The sample spectral components are then compared with characteristic low-frequency spectral components of known compounds suspected of being present in the sample. In a typical example, the sample components are compared against the data set of each of the components suspected of being in the sample and which one desires to detect. A components, e.g., compound is identified as being present in the sample if one or more of its characteristic low-frequency spectral components correspond to one or more low-frequency spectral components of a known sample.

[00192] As shown in the set of Figures 11A-11F, detection of a compound (an amino acid) can occur at very low levels, e.g., in the parts per billion range or lower. In particular, even at a dilution of 1:10 billion w/v, a characteristic spectral component at about 531 Hz is observed. The Figures demonstrate that signal amplitude, corresponding spectral component correlation, does decline with increasing compound dilution. However, the loss in signal amplitude at low concentration can be compensated for by extending the recording time, in this example, from 50 seconds for the first group of Figures to 4.25 minutes for the most dilute sample (Figure 11F).

[00193] Where, as in the above example, the spectral component amplitude declines with decreasing concentration, the amount of compound can be estimated on the basis of signal amplitude, assuming that the data set for the compound also includes concentration dependent amplitude information.

[00194] It has also been observed in some cases that the frequency of the characteristic spectral components may shift by as much as 3 Hz in a systematic fashion with changes in concentration. For such compounds, the amount of material present in a sample can be estimated by changes in amplitude and/or frequency shift in one or more of the spectral components. It will be appreciated for materials showing a concentration dependent frequency shift that a data set for that compound could include concentration-dependent frequencies as well as concentration-dependent amplitudes for particular components.

#### D. Time-domain signals

[00195] In still another aspect, the invention includes a time-domain signal associated with a material of interest. The time-domain signal, and its method of production, have been discussed above. Briefly, the signal is produced by placing the sample of interest in a container having both magnetic and electromagnetic shielding, injecting Gaussian noise into the sample; and recording an electromagnetic time-domain signal composed of sample source radiation superimposed on the injected Gaussian noise.

[00196] The signal may be used to characterize a sample, much as a spectral component data set is used to characterize a material. Alternatively, the signal may be used for generating a low frequency signal signature of spectral components associated with a material of interest. The signal signature can be generated, also as described above, by (i) cross correlating the time-domain signal recorded with a second time domain signal separately recorded from the same or similar sample, to produce a frequency domain spectrum in a frequency range within DC to 50 kHz.

#### Conclusion

[00197] Unless the context clearly requires otherwise, throughout the description and the claims, the words "comprise," "comprising," and the like are to be construed in an inclusive sense as opposed to an exclusive or exhaustive sense; that is to say, in the sense of "including, but not limited to." Words in the above detailed description using the singular or plural number may also include the plural or singular number respectively. Additionally, the words "herein," "above," "below" and words of similar import, when used in this application, shall refer to this application as a whole and not to any particular portions of this application. When the claims use the word "or" in reference to a list of two or more items, that word covers all of the following interpretations of the word: any of the items in the list, all of the items in the list and any combination of the items in the list.

[00198] The above detailed descriptions of embodiments of the invention are not intended to be exhaustive or to limit the invention to the precise form disclosed above. While specific embodiments of, and examples for, the invention are described above for illustrative purposes, various equivalent modifications are possible within the scope of the invention, as those skilled in the relevant art will recognize. For example, while processes or steps are presented in a given order, alternative embodiments may perform routines having steps in a different order, and

some steps may be deleted, moved, added, subdivided, combined, and/or modified. Each of these steps may be implemented in a variety of different ways. Also, while these steps are shown as being performed in series, these steps may instead be performed in parallel, or may be performed at different times.

[00199] The teachings of the invention provided herein can be applied to other systems, not necessarily the system described herein. These and other changes can be made to the invention in light of the detailed description. The elements and acts of the various embodiments described above can be combined to provide further embodiments.

[00200] All of the above patents and applications and other references, including any that may be listed in accompanying filing papers, are incorporated herein by reference. Aspects of the invention can be modified, if necessary, to employ the systems, functions and concepts of the various references described above to provide yet further embodiments of the invention.

[00201] These and other changes can be made to the invention in light of the above detailed description. While the above description details certain embodiments of the invention and describes the best mode contemplated, no matter how detailed the above appears in text, the invention can be practiced in many ways. Details of the signal acquiring and analysis system may vary considerably in its implementation details, while still be encompassed by the invention disclosed herein. As noted above, particular terminology used when describing certain features or aspects of the invention should not be taken to imply that the terminology is being re-defined herein to be restricted to any specific characteristics, features or aspects of the invention with which that terminology is associated. In general, the terms used in the following claims should not be construed to limit the invention to the specific embodiments disclosed in the specification, unless the above Detailed Description section explicitly defines such terms. Accordingly, the actual scope of the invention encompasses not only the disclosed embodiments, but also all equivalent ways of practicing or implementing the invention under the claims.

[00202] While certain aspects of the invention are presented below in certain claim forms, the inventors contemplate the various aspects of the invention in any number of claim forms. For example, while only one aspect of the invention is recited as embodied in a method claim format, it may likewise be embodied in a computer-readable medium claim format. Accordingly, the inventors reserve the

right to add additional claims after filing the application to pursue such additional claim forms for other aspects of the invention.

## CLAIMS

I/We claim:

1. Apparatus for interrogating a sample that exhibits low-frequency molecular motion, comprising:

- a container adapted for receiving the sample, the container having both magnetic and electromagnetic shielding;
- an adjustable-power source of Gaussian noise for directing Gaussian noise to the sample, with the sample in the container;
- a detector for detecting an electromagnetic time-domain signal composed of sample source radiation superimposed with the directed Gaussian noise; and
- an electronic computer adapted to receive the time-domain signal from the detector, and to process the signal to generate a spectral plot that displays, at a selected power setting of the Gaussian noise source, low-frequency spectral components characteristic of the sample in a selected frequency range between DC and 50 kHz.

2. The apparatus of claim 1, wherein the electronic computer includes a signal analyzer that functions to (i) calculate a series of Fourier spectra of the time-domain signal over each of a plurality of defined time periods, in a selected frequency range between 100 Hz and 50 kHz, and (ii) average the Fourier spectra.

3. The apparatus of claim 2, wherein the calculating includes calculating at least five Fourier spectra, each taken over a 1-5 second time-domain interval.

4. The apparatus of claim 1, wherein the electronic computer includes machine readable code operable to:

- (i) store the time-domain signal of the sample over a sample-duration time  $T$ ;
- (ii) select a sampling rate  $F$  for sampling the time domain signal, where  $F \cdot T$  is a total sample count  $S$ ,  $F$  is approximately twice a frequency

domain resolution  $f$  of a Real Fast Fourier Transform of the time-domain signal sampled at sampling rate  $F$ , and  $S > f * n$ , where  $n$  is at least 10,

- (iii) select  $S/n$  samples from the stored time domain signal and perform a Real Fast Fourier Transform (RFFT) on the selected samples to produce an RFFT signal,
- (iv) normalize the RFFT signal and calculate an average power for the RFFT signal,
- (v) place an event count in each of  $f$  selected-frequency event bins where a measured power at a corresponding selected frequency is greater than an average power times a value  $\epsilon$ , where  $0 < \epsilon < 1$  and is chosen such that a total number of counts placed in an event bin is between about 20-50% of a maximum possible bin counts in that bin,
- (vi) repeat steps (iii-v), and
- (viii) generate a histogram that shows, for each event bin  $f$  over a selected frequency range, a number of event counts in each bin.

5. The apparatus of claim 4, wherein the machine readable code is further operable to, in (iv), place the normalized power value from the RFFT signal in  $f$  corresponding-frequency power bins, and in (viii), (a) divide accumulated values placed in each of the  $f$  power bins by  $n$ , to yield an average power in each bin, and (b) display in the histogram, the average power in each bin.

6. The apparatus of claim 4, wherein the machine readable code is further operable to, in (viii), identify those bins in the histogram that have an event count above a given threshold and an average power.

7. The apparatus of claim 1, wherein the source of Gaussian noise includes an adjustable-power Gaussian noise generator and a Helmholtz coil which is contained within the magnetic electromagnetic shielding, and which receives a selected noise output signal from the noise generator in a range 100 mV to 1 V.

8. The apparatus of claim 7, wherein the generator is designed to inject Gaussian noise into the sample at a frequency between DC and 2 kHz.

9. The apparatus of claim 1, wherein the detector is a second-derivative gradiometer which outputs a current signal, and a SQUID operatively connected to the gradiometer to convert the current signal to an amplified voltage signal.

10. The apparatus of claim 9, wherein the container is an attenuation tube having a sample-holding region, a magnetic shielding cage surrounding the region, and a Faraday cage also surrounding the region, wherein the source of Gaussian noise includes a Gaussian noise generator and a Helmholtz coil, wherein the Helmholtz coil is contained within the magnetic cage and the Faraday cage and receives a noise output signal from the noise generator, and wherein the apparatus further includes, for use in removing stationary noise components, a signal inverter operatively connected to the noise generator and to the SQUID, for receiving Gaussian noise from the noise generator and outputting into the SQUID, Gaussian noise in inverted form with respect to the Gaussian noise injected to the sample.

11. A method for interrogating a sample that exhibits low-frequency molecular motion, comprising:

placing the sample in a container having both magnetic and electromagnetic shielding,

- (a) injecting Gaussian noise into the sample at a selected noise amplitude;
- (b) recording an electromagnetic time-domain signal composed of sample source radiation superimposed on the injected Gaussian noise,
- (c) generating a spectral plot that contains, at a selected power setting of the Gaussian noise source, low-frequency, sample-dependent spectral components characteristic of the sample in a selected frequency range between 100 and 50 kHz, and

- (d) repeating (a)-(c) at different selected noise amplitudes until a plot showing a maximum or near maximum number of spectral components characteristic of the sample is generated.

12. The method of claim 11, wherein the generating includes (i) calculating a series of Fourier spectra of the time-domain signal over each of a plurality of defined time periods, in a selected frequency range between 100 Hz and 50 kHz, and (ii) averaging the Fourier spectra.

13. The method of claim 12, wherein the calculating includes:

- (i) storing a time-domain signal of the sample over a sample-duration time  $T$ ;
- (ii) selecting a sampling rate  $F$  for sampling the time-domain signal, where  $F * T$  is a total sample count  $S$ ,  $F$  is approximately twice a frequency domain resolution  $f$  of a Real Fast Fourier Transform of the time-domain signal sampled at the sampling rate  $F$ , and  $S > f * n$ , where  $n$  is at least 10,
- (iii) selecting  $S/n$  samples from the stored time-domain signal and performing a Real Fast Fourier Transform (RFFT) on the selected samples to produce an RFFT signal,
- (iv) normalizing the RFFT signal and calculating an average power for the RFFT signal,
- (v) placing an event count in each of  $f$  selected-frequency event bins where a measured power at a corresponding selected frequency  $>$  average power  $* \epsilon$ , where  $0 < \epsilon < 1$  and is chosen such that a total number of counts placed in an event bin is between about 20-50% of a maximum possible bin count in that bin,
- (vi) repeating (iii) through (v), and
- (viii) generating a histogram that shows, for each event bin  $f$  over a selected frequency range, a number of event counts in each bin.

14. The method of claim 13, which further includes, in (iv) placing the normalized power value from the RFFT signal in  $f$  corresponding-frequency power

bins, and in (viii): (a) dividing accumulated values placed in each of the  $f$  power bins by  $n$ , to yield an average power in each bin, and (b) displaying on the histogram, the average power in each bin.

15. The method of claim 14, which further includes identifying those bins in the histogram that have an event count above a given threshold and an average power.

16. A method of characterizing spectral emission features of a sample material, over a selected frequency range  $R$ , comprising:

selecting  $S/n$  samples from a time-domain signal and performing a Fast Fourier Transform (FFT) on the samples to produce an FFT signal, wherein  $F$  is a sampling rate for sampling the time-domain signal, where  $F \cdot T$  is a total sample count  $S$ ,  $F$  is greater than a frequency domain resolution  $f$  of the FFT of the time-domain signal sampled at the sampling rate  $F$ , and  $S > f \cdot n$ , where  $n$  is at least 5;

calculating an average power for the FFT signal,

placing an event count in each of  $f$  selected-frequency event bins where the measured power at the corresponding selected frequency  $>$  average power  $\cdot \epsilon$ , where  $0 < \epsilon < 1$  and is chosen such that the total number of counts placed in an event bin is between about 20-50% of maximum possible bin counts in that bin; and

generating a display that shows, for each event bin  $f$  over a selected frequency range, a number of event counts in each bin.

17. The method of claim 16, which further includes normalizing the FFT signal before calculating the average power, placing the normalized power value from the FFT in  $f$  corresponding-frequency power bins, dividing accumulated values placed in each of the  $f$  power bins by  $n$  to yield an average power in each bin, and displaying on a histogram the average power in each bin.

18. The method of claim 17, which further includes identifying those bins in the histogram that have an event count above a given threshold and an average power.

19. The method of claim 18, wherein  $R$ , expressed in Hz, is approximately equal to  $f$ , and the sample rate  $F$ , expressed in samples/second, is approximately  $2f$ .

20. The method of claim 19, wherein the method detects low-frequency emission events related to molecular emissions in a sample, and wherein  $R$  includes at least the frequency range of 100 Hz to 5 kHz.

21. The method of claim 16, further comprising normalizing the FFT signal before calculating the average power, and wherein the FFT is a Real Fast Fourier Transform.

22. The method of claim 16, further comprising before, selecting, storing a time-domain signal of the sample over a sample-duration time  $T$ ;

23. The method of claim 16, further comprising repeating the selecting, calculating and placing, before generating the display.

24. A low-frequency spectral signature associated with a material of interest comprising:

a list of frequency components in the DC-50 kHz frequency range that are generated by the method of claim 16.

25. The spectral signature of claim 24, wherein the frequencies in the list are identified from a histogram of a number of sample-dependent stochastic events occurring at each of a plurality of spectral increments within a selected frequency range between DC and 50 kHz.

26. An apparatus for detecting molecular signals from a sample, wherein the sample acts as a signal source, the apparatus comprising:

means for detecting electromagnetic emissions positioned near to the sample;

a Super Conducting Quantum Interference Device electrically connected to the means for detecting, wherein the Super Conducting Quantum Interference Device is positioned within a means for cryogenically cooling;

noise generation means for surrounding the signal source and the means for detecting signals with structured or uniform noise;

means for electromagnetically shielding the signal source, means for detecting, and Super Conducting Quantum Interference Device from external electromagnetic radiation, and wherein the means for electromagnetically shielding is positioned exterior to the means for cryogenically cooling;

means for controlling the Super Conducting Quantum Interference Device; and

means for observing the signal detected by the means for detecting electromagnetic emissions.

27. The apparatus of claim 26, further comprising tube means for vertically receiving the signal source therein, wherein the tube means provides at least 2 kHz of low pass filtering.

28. The apparatus of claim 26, further comprising automatic loading means for automatically and vertically positioning the signal source within the apparatus.

29. The apparatus of claim 26, further comprising superconducting lead shielding that at least partially encloses the signal source and means for detecting.

30. The apparatus of claim 26 wherein the means for detecting includes a second derivative gradiometer.

31. A computer-readable medium whose contents cause at least one data processing device to perform a method to display data representing electromagnetic emissions from a sample, the method comprising:

receiving a sample signal that has been produced by applying noise to a sample within a magnetically shielded detection apparatus, wherein a combination of the noise with an electromagnetic signal emitted by the sample takes on a different characteristic than the noise through stochastic resonance, and wherein the magnetically shielded detection apparatus includes therein a Super Conducting Quantum Interference Device electrically connected to at least one electromagnetic emission detection coil;

applying a Fast Fourier Transform to the sample signal; and

displaying, via a graphical user interface, the sample signal, wherein the sample signal is displayed as a series of peaks at select frequencies, wherein the peaks are substantially greater than other peaks in the sample signal, and wherein at least some of the other peaks represent the noise.

32. The computer-readable medium of claim 31 wherein the computer-readable medium is a memory of the data processing device.

33. The computer-readable medium of claim 31 wherein the computer-readable medium is a logical node in a computer network receiving the contents.

34. The computer-readable medium of claim 31 wherein the computer-readable medium is a computer-readable disk.

35. The computer-readable medium of claim 31 wherein the computer-readable medium is a data transmission medium carrying a generated data signal containing the contents.

36. The computer-readable medium of claim 31 wherein the computer-readable medium is a memory of a computer system.

37. An apparatus for detecting molecular signals from a sample, wherein the sample acts as a signal source, the apparatus comprising:

an electromagnetic emissions detector positioned near to the sample for detecting an emissions signal from the signal source;

a Super Conducting Quantum Interference Device (SQUID) electrically connected to the electromagnetic emissions detector, wherein the Super Conducting Quantum Interference Device is cryogenically cooled;

a noise canceling component;

a noise generator for providing structured or uniform noise to the emissions signals from the signal source, and for providing an inverted version of the noise to the noise canceling component;

electromagnetic shielding configured to shield the signal source, electromagnetic emissions detector, and Super Conducting Quantum Interference Device from external electromagnetic radiation;

a controller for controlling the Super Conducting Quantum Interference Device; and

an output port for outputting an amplified emissions signal, wherein the amplified emissions signal represents amplification of the signal source signal, through stochastic resonance, by the noise.

38. The apparatus of claim 37 wherein the noise canceling component is positioned between the electromagnetic emissions detector and an input to the SQUID.

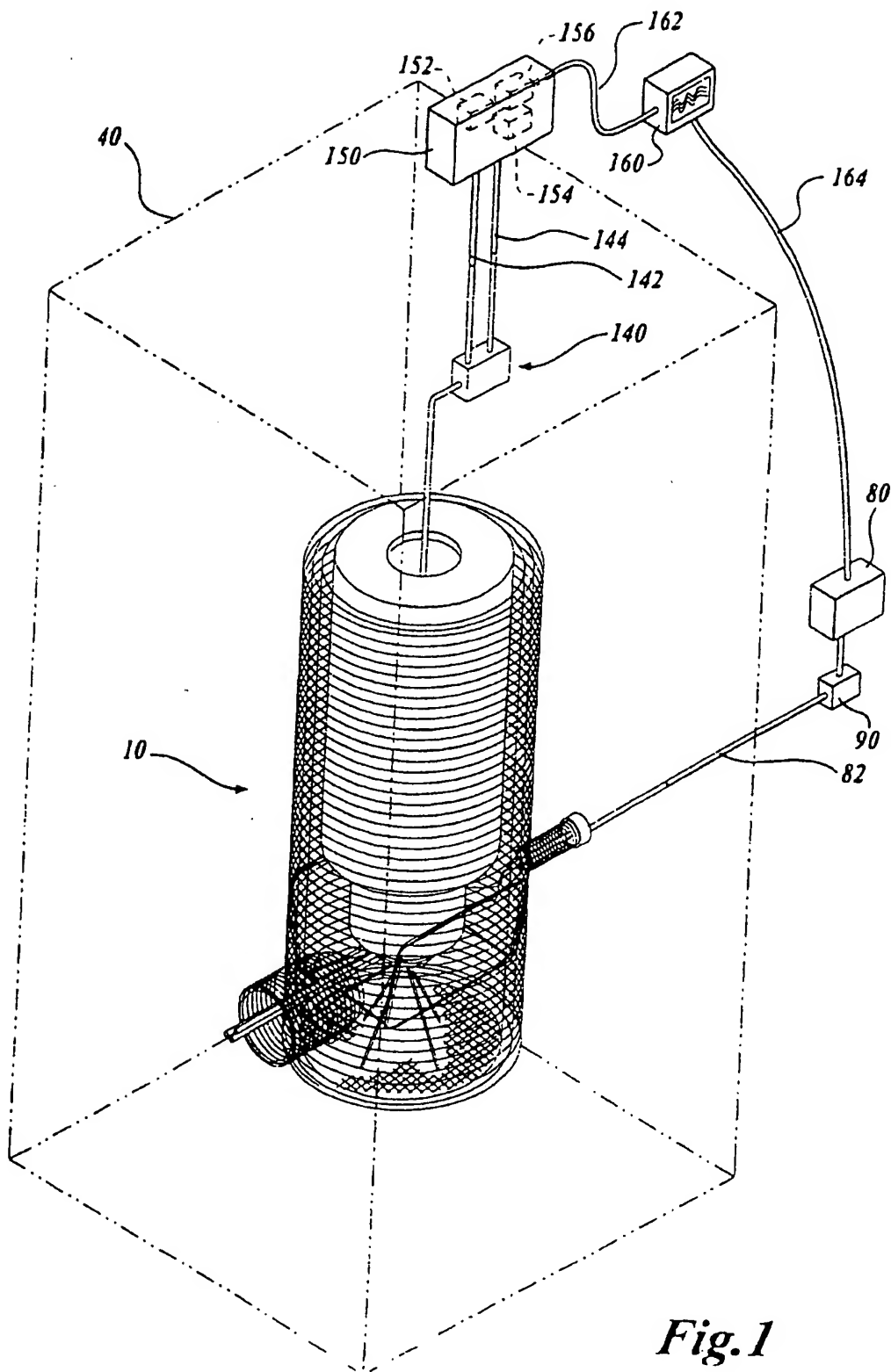
39. The apparatus of claim 37 wherein the noise canceling component is positioned between the electromagnetic emissions detector and an output to the SQUID.

40. The apparatus of claim 37 wherein the noise generator includes first and second noise generating components, and noise canceling component includes first and second noise canceling components, the wherein the first noise canceling

component is positioned between the electromagnetic emissions detector and an input to the SQUID and is coupled to the first noise generator, and wherein the second noise canceling component is positioned at an output of the SQUID and is coupled to the second noise generator.

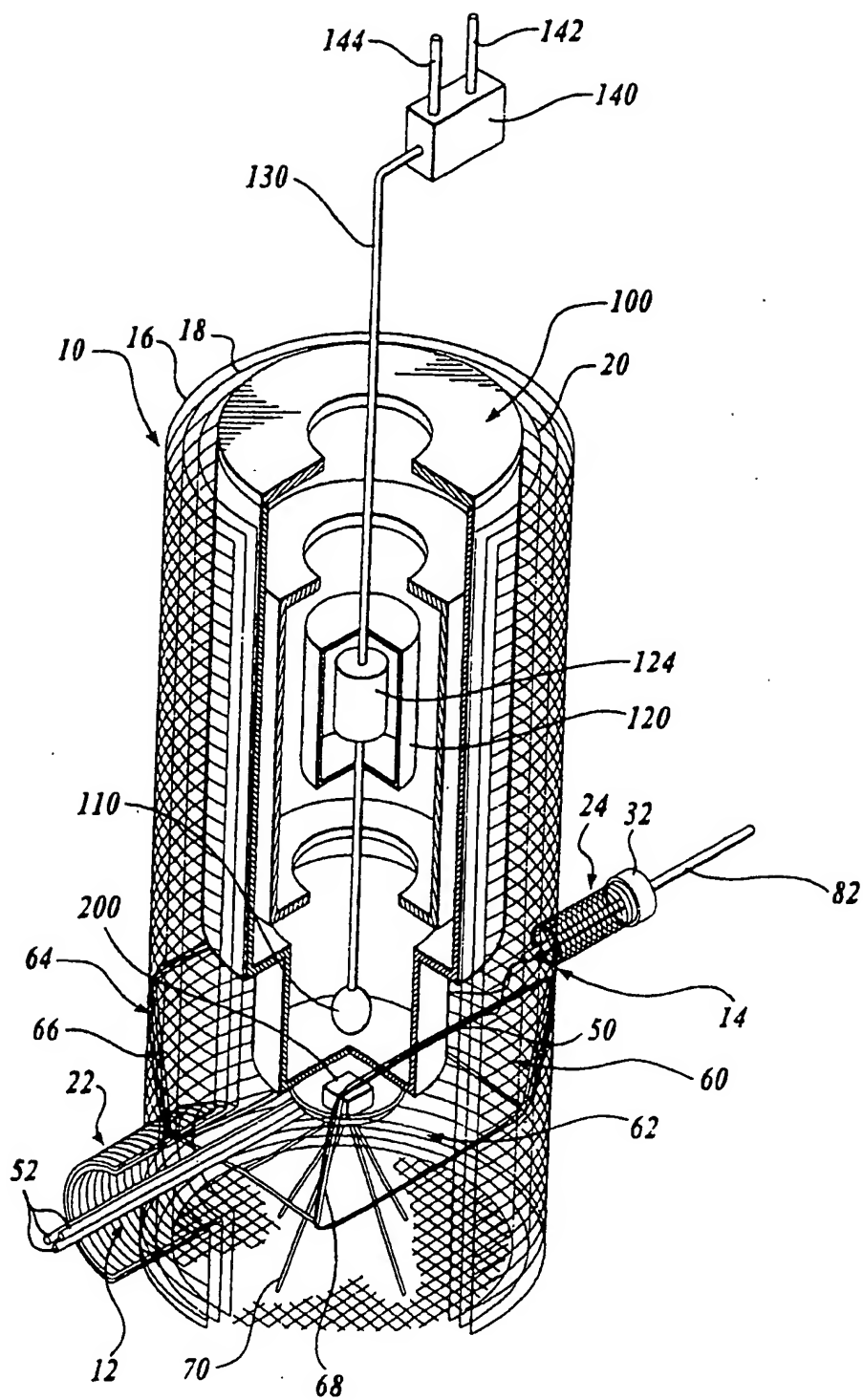
41. The apparatus of claim 37 wherein the noise generator provides a series of random values from a random number generator, and wherein the noise canceling component subtracts the series of random values from the amplified emissions signal.

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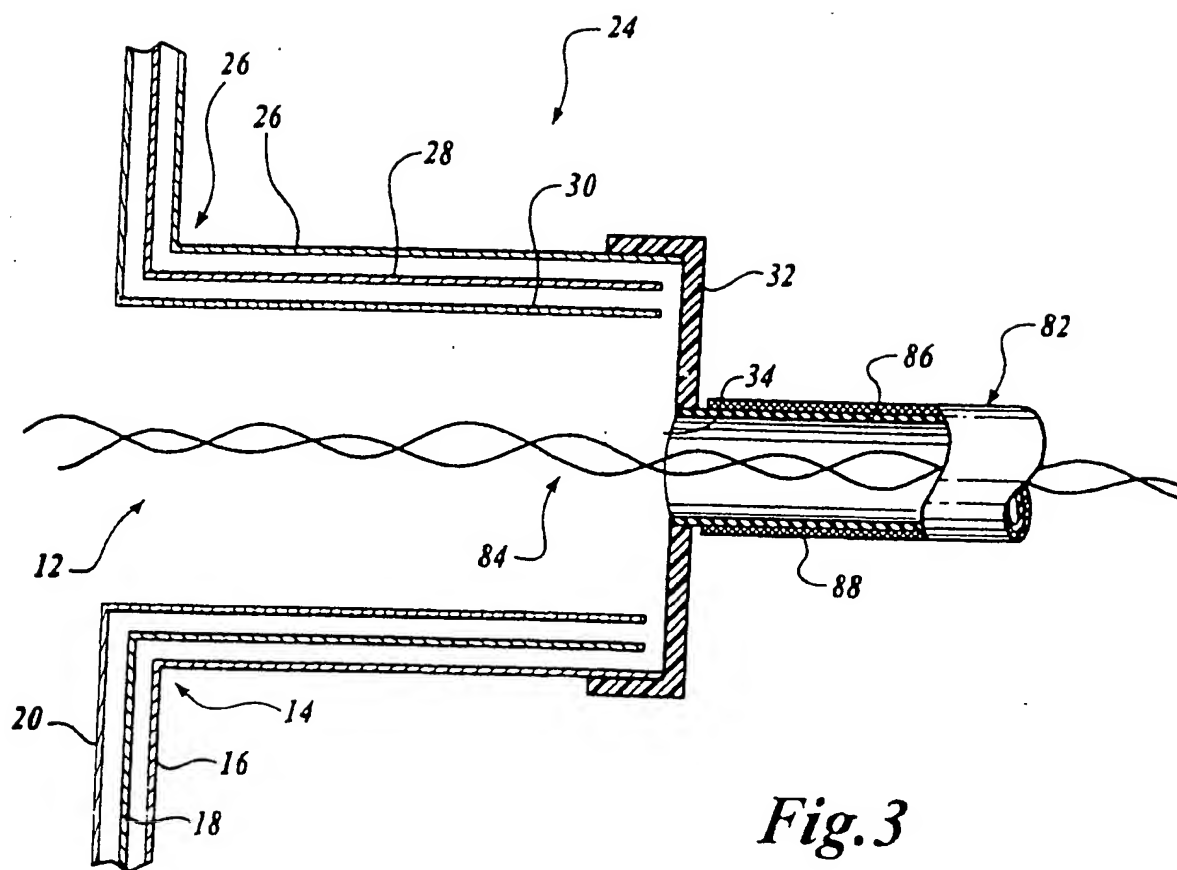


*Fig. 1*

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*Fig. 2*

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*Fig. 3*

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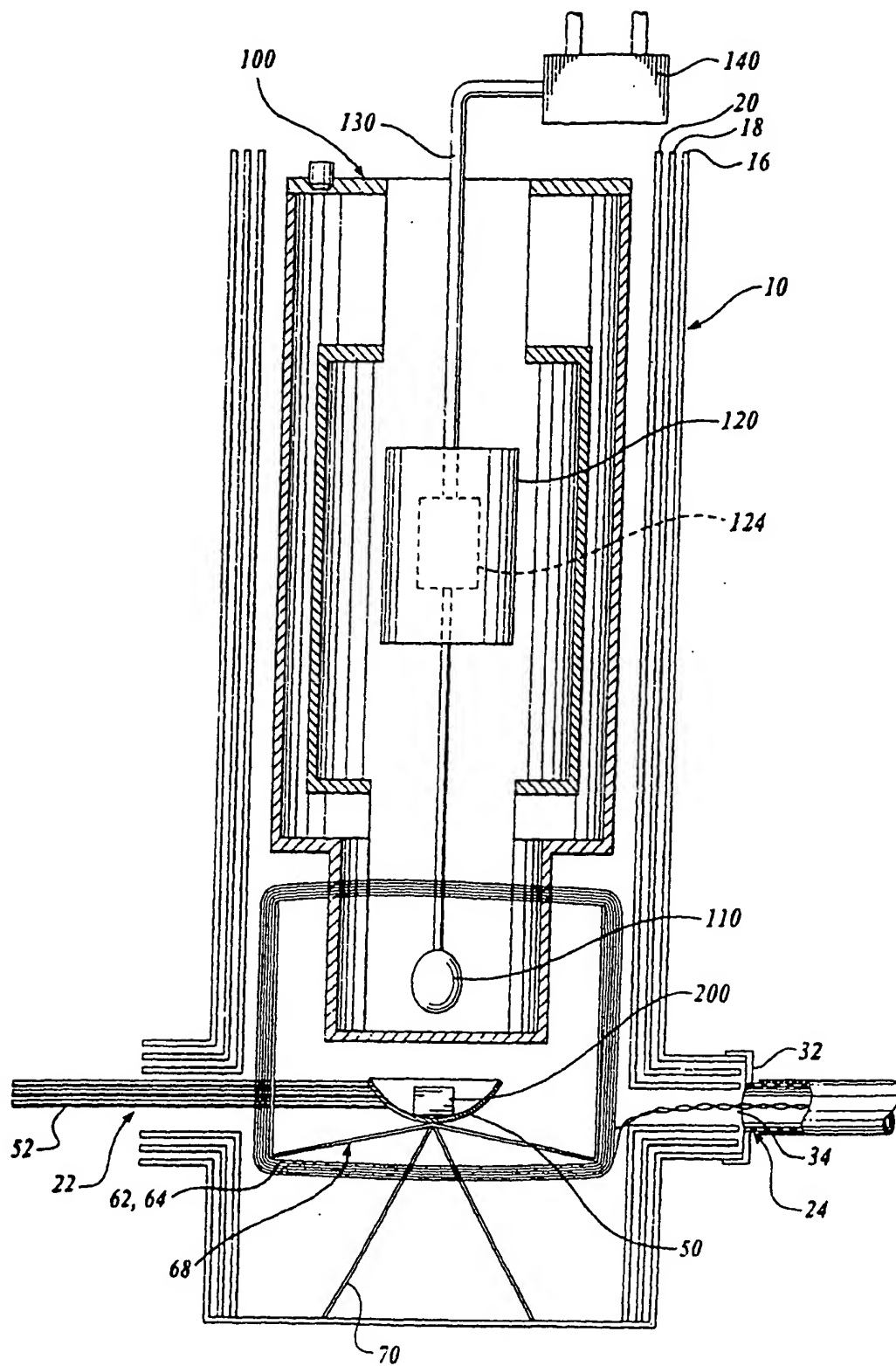
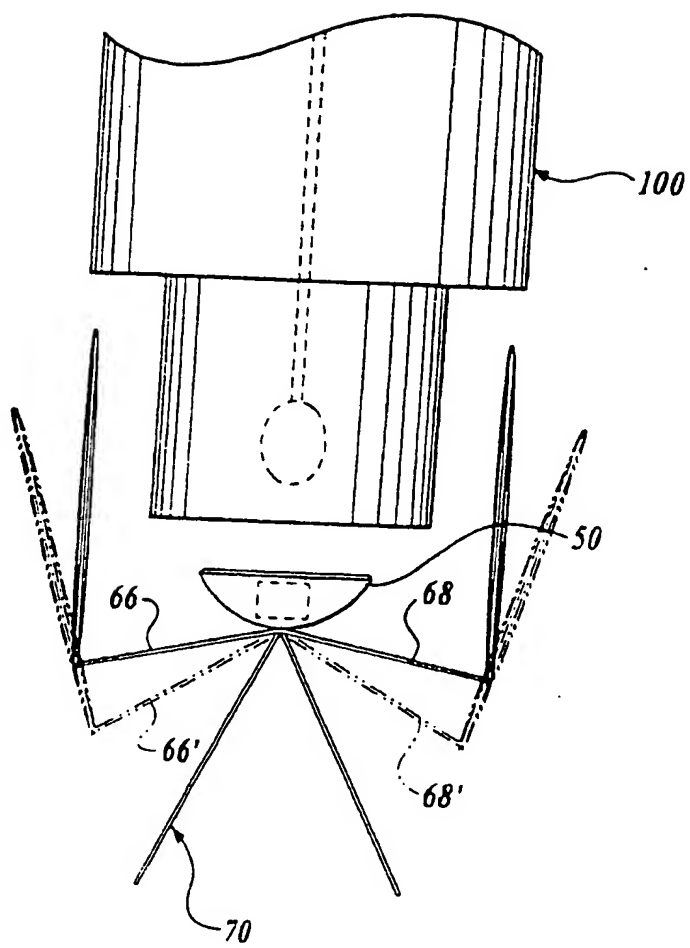


Fig. 4



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*Fig. 6*

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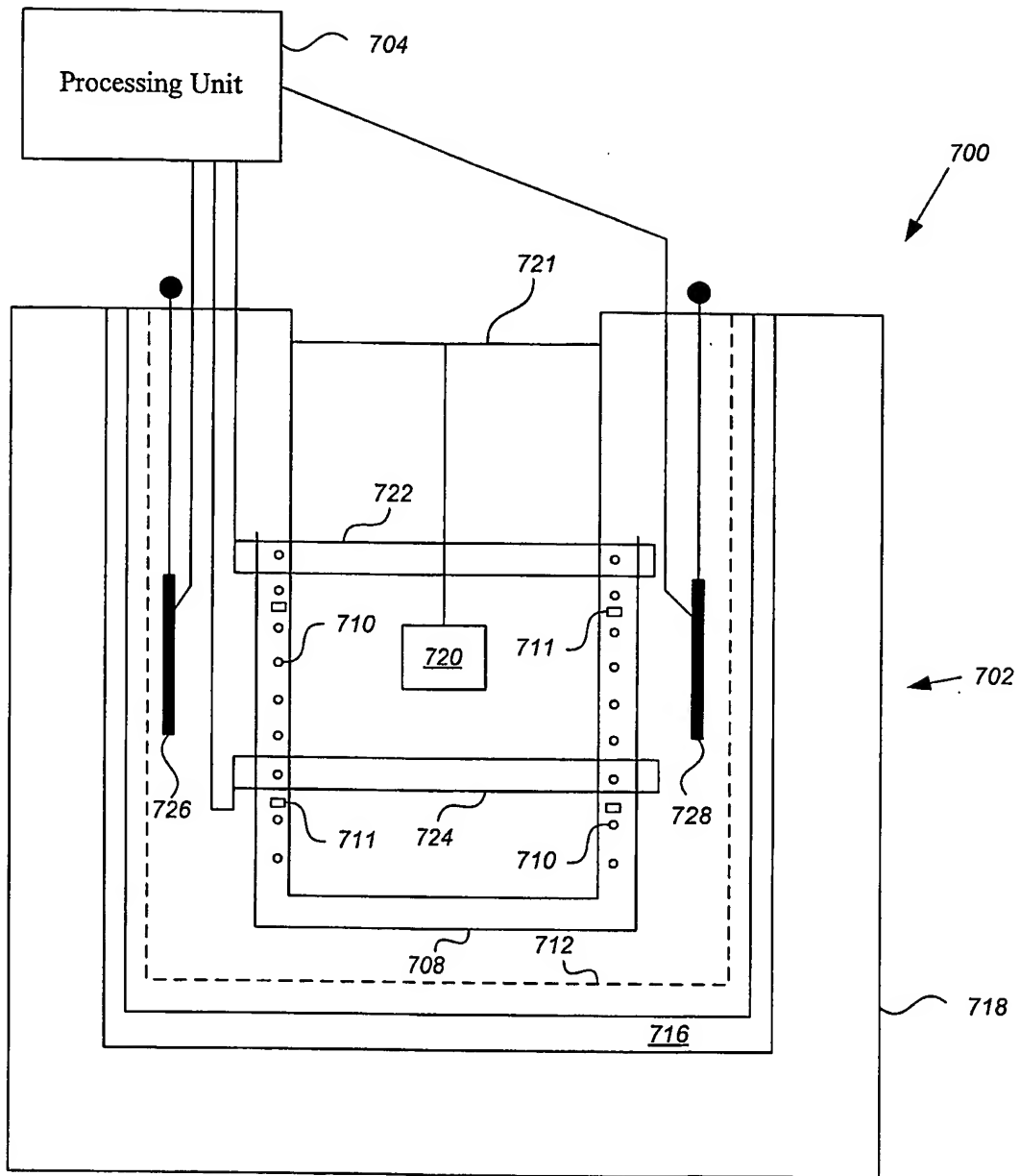


FIG. 7

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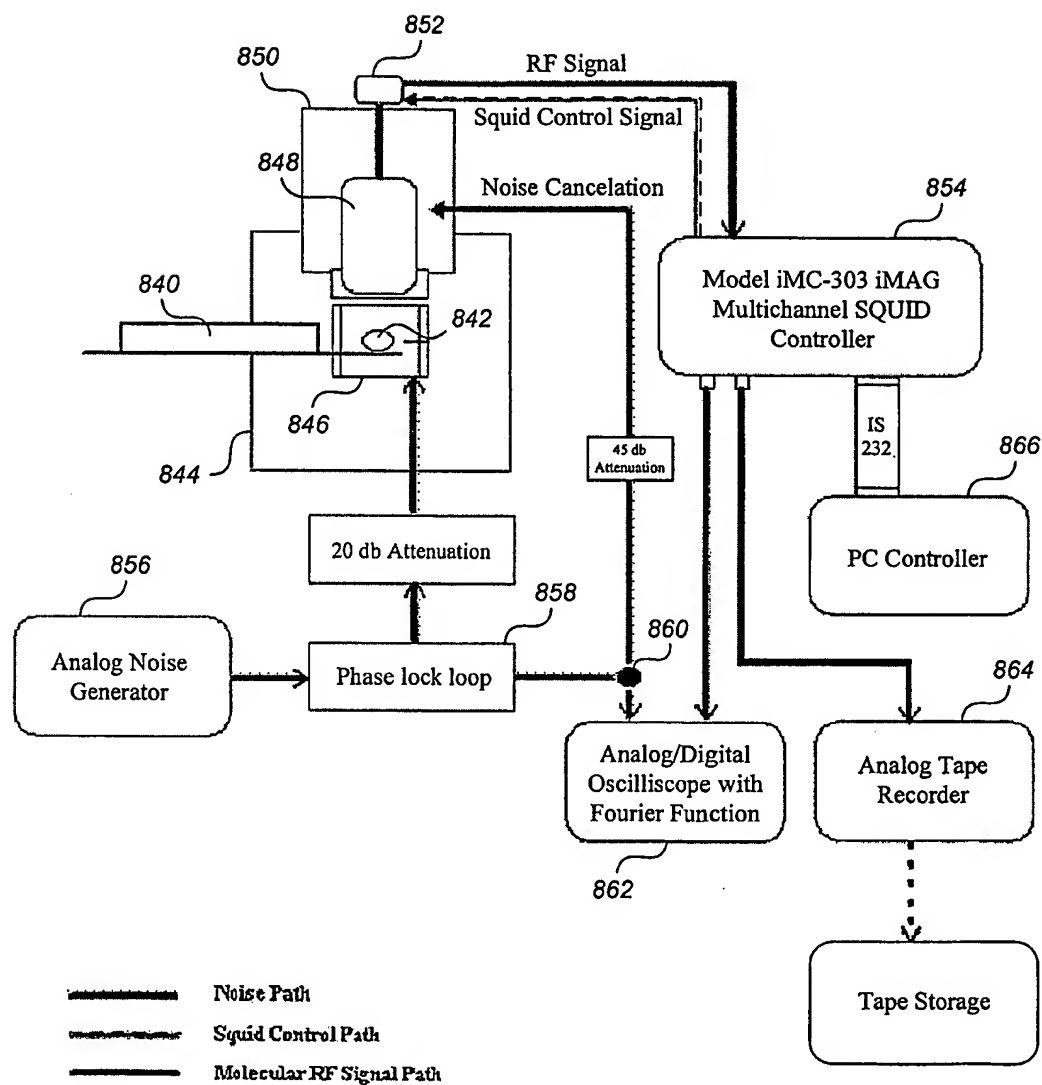


FIG. 8

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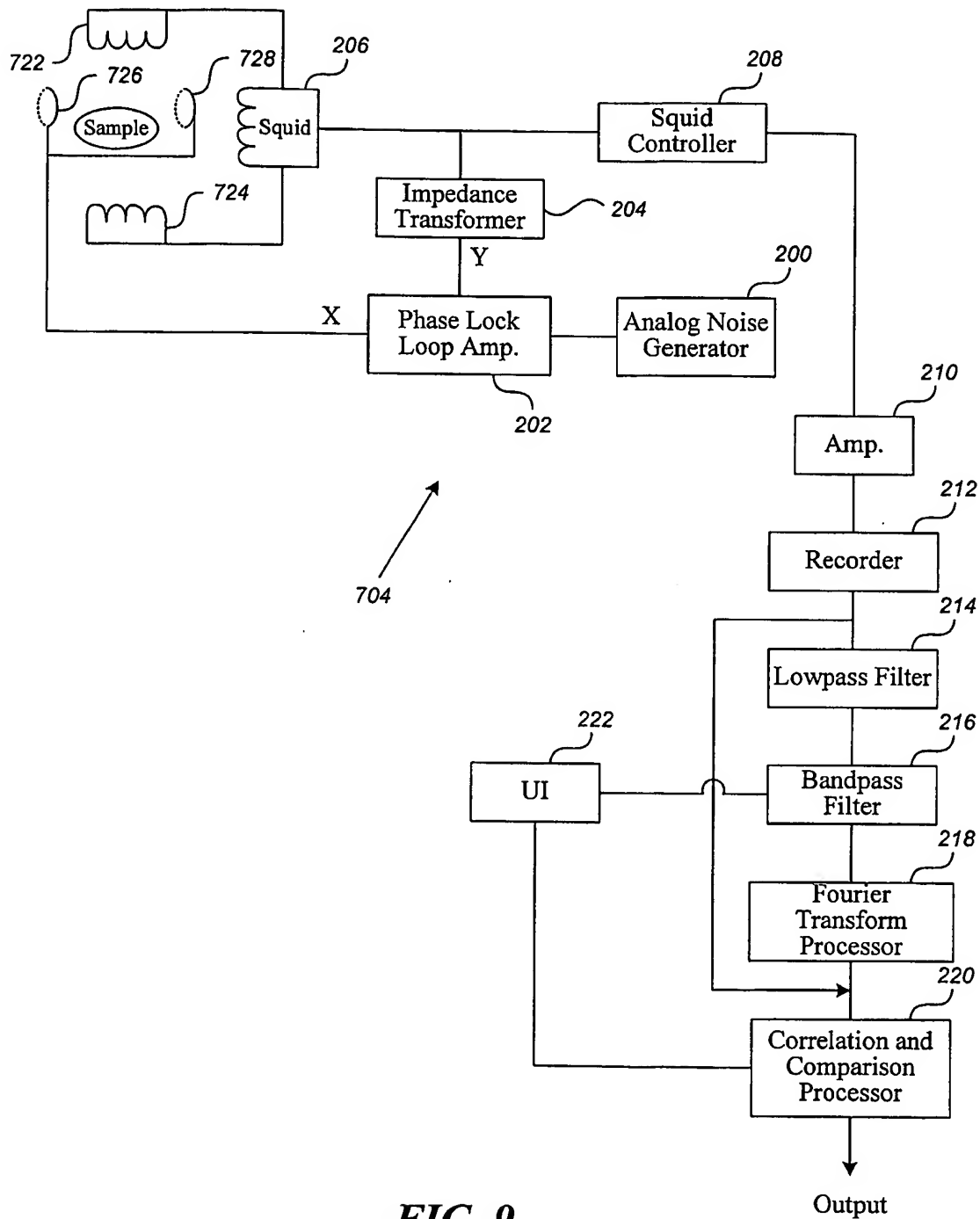
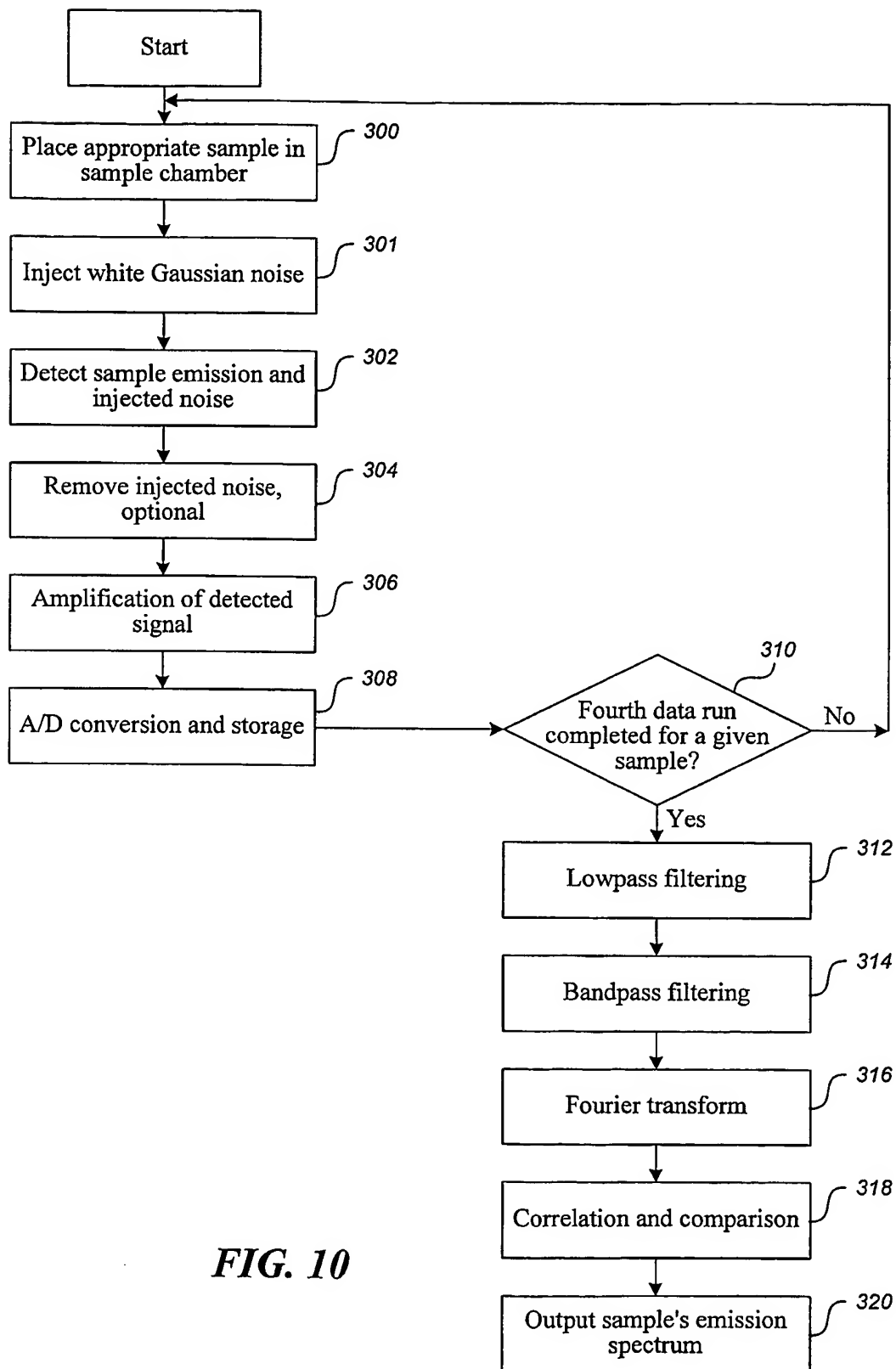
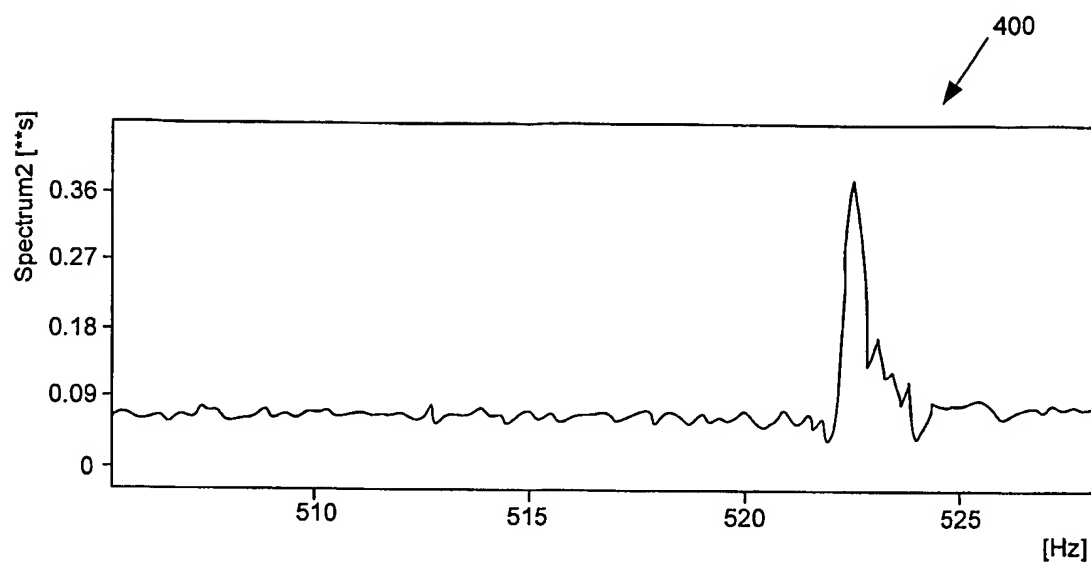
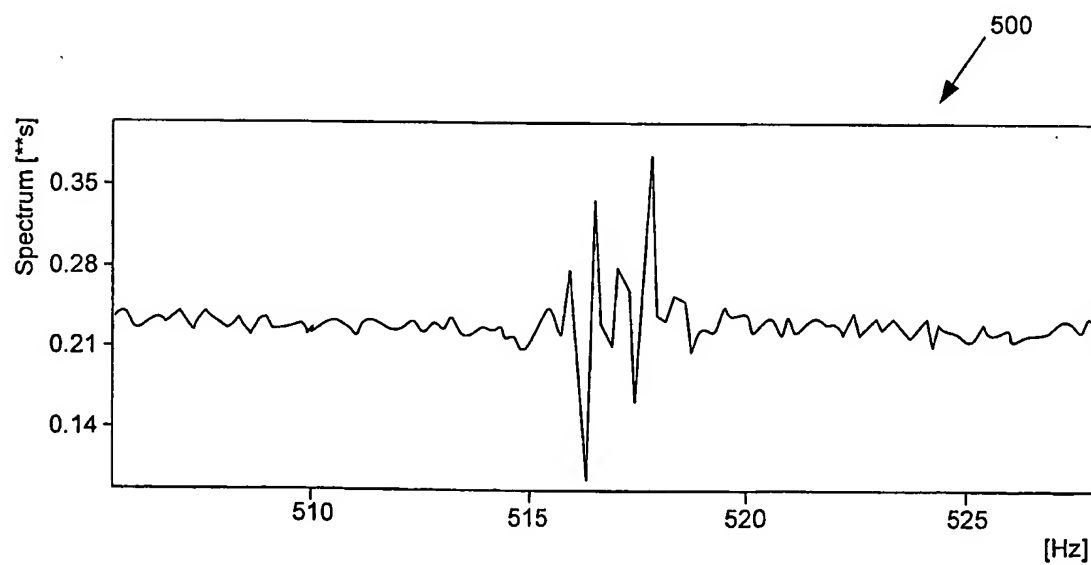


FIG. 9

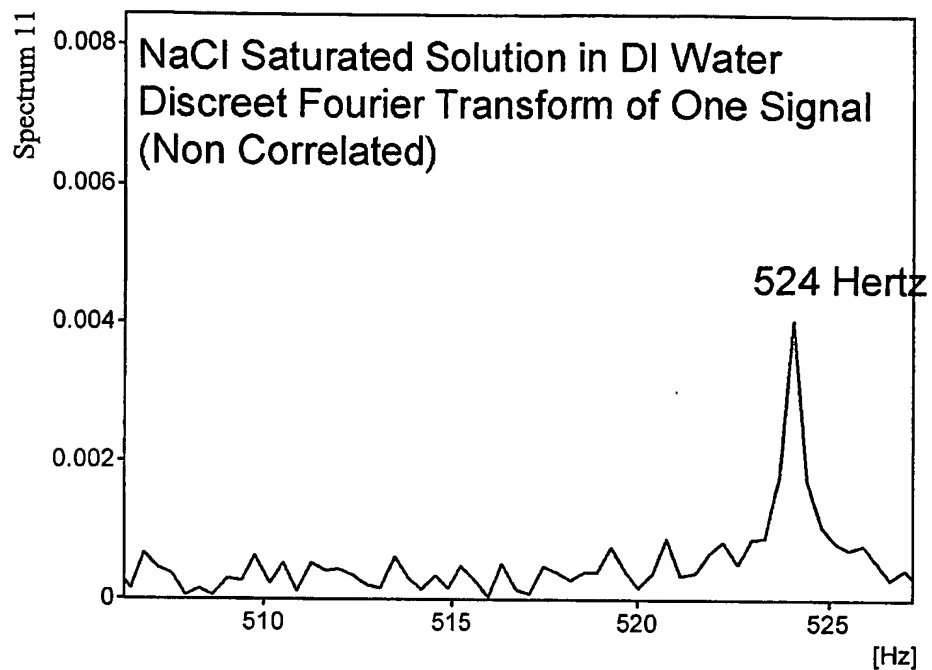
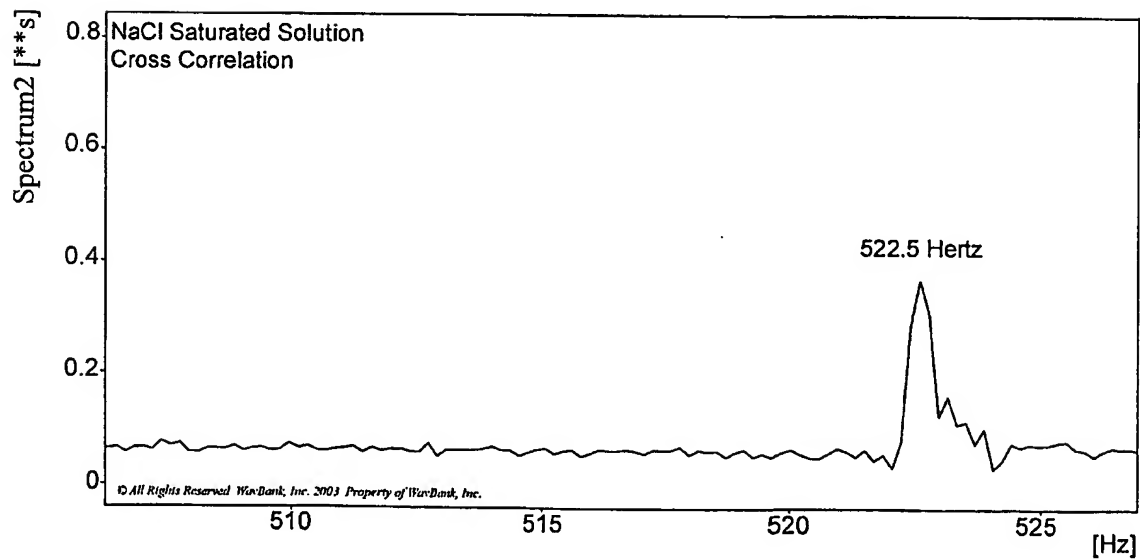
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**FIG. 10**

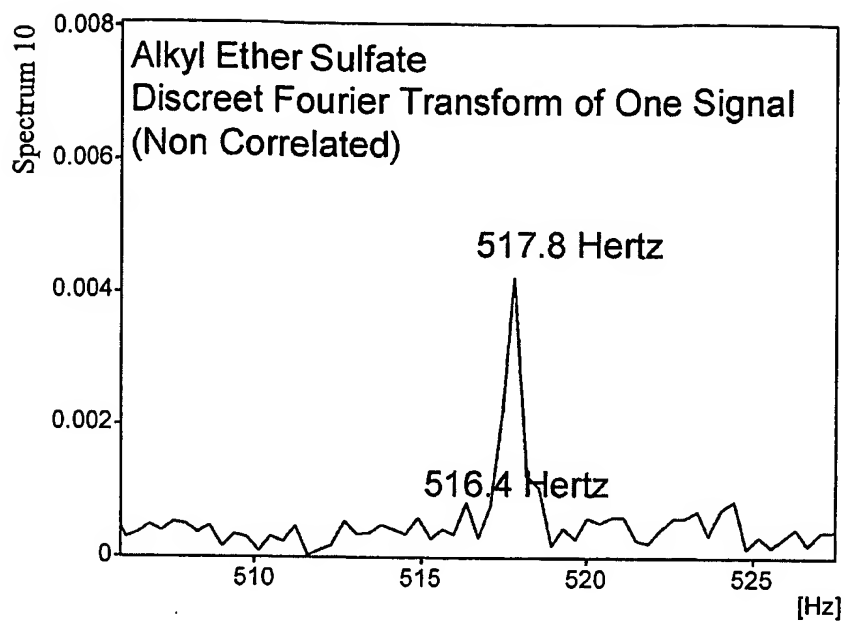
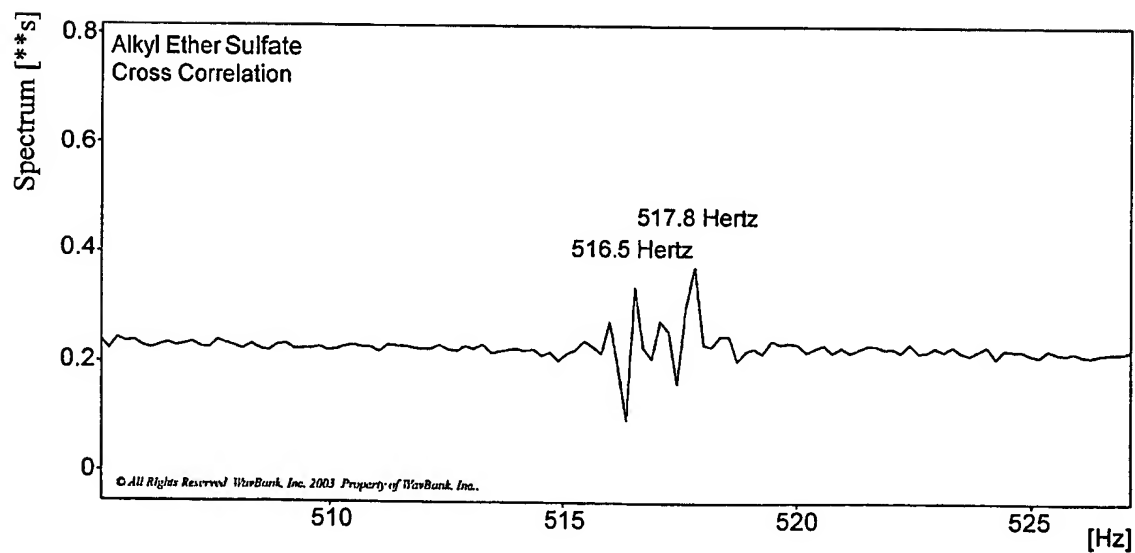
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**FIG. 11A****FIG. 11B**

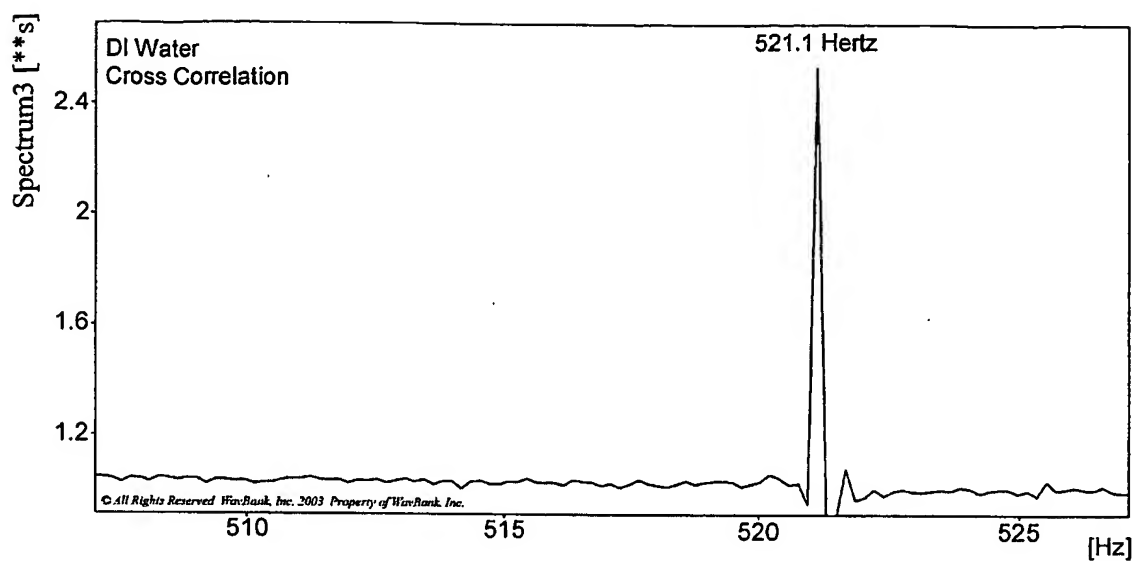
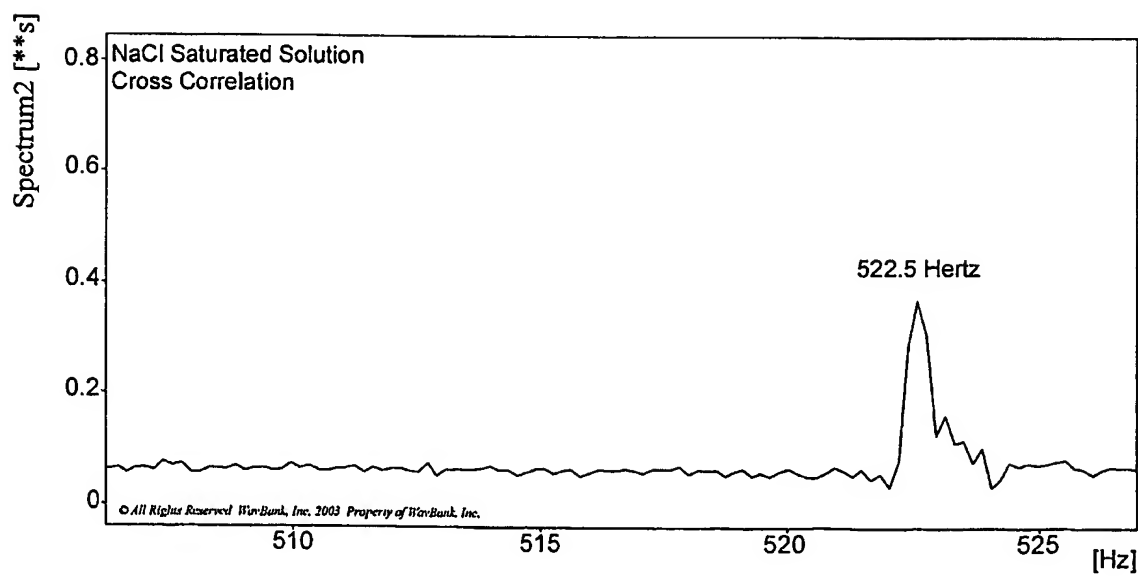
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**FIG. 12A****FIG. 12B**

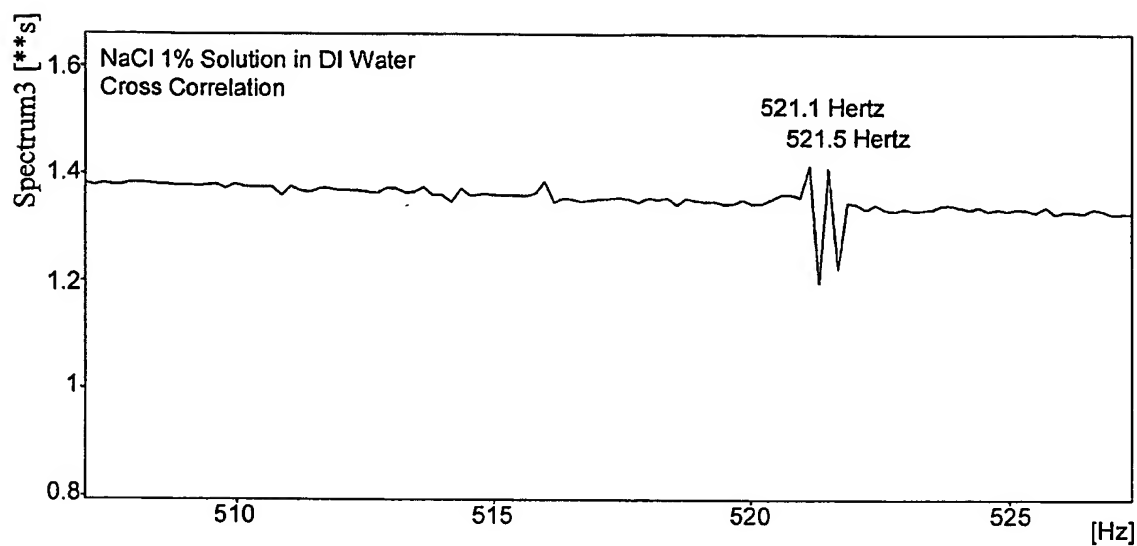
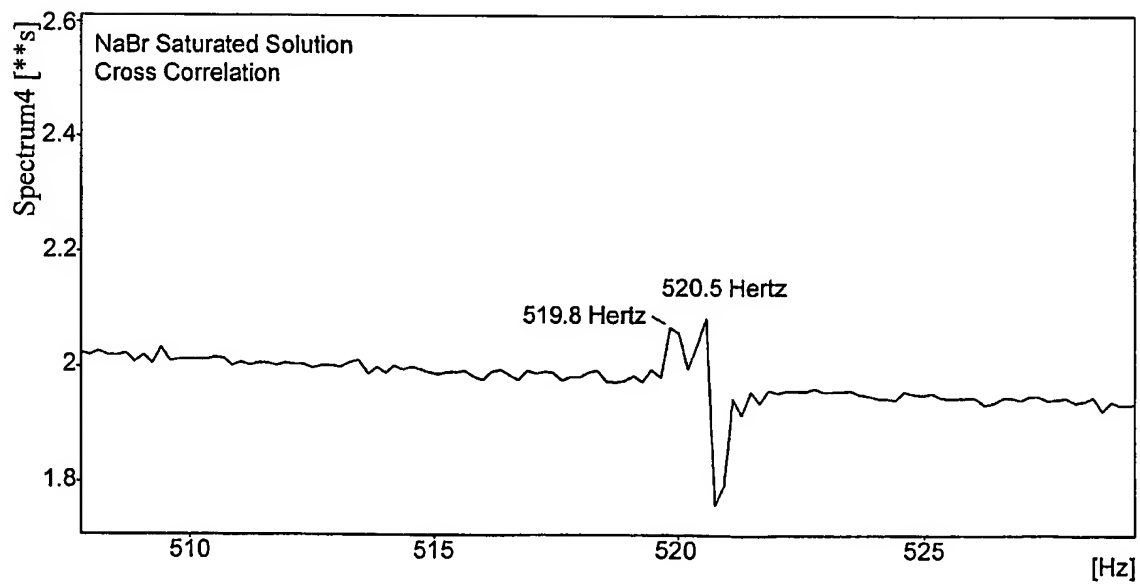
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**FIG. 13A****FIG. 13B**

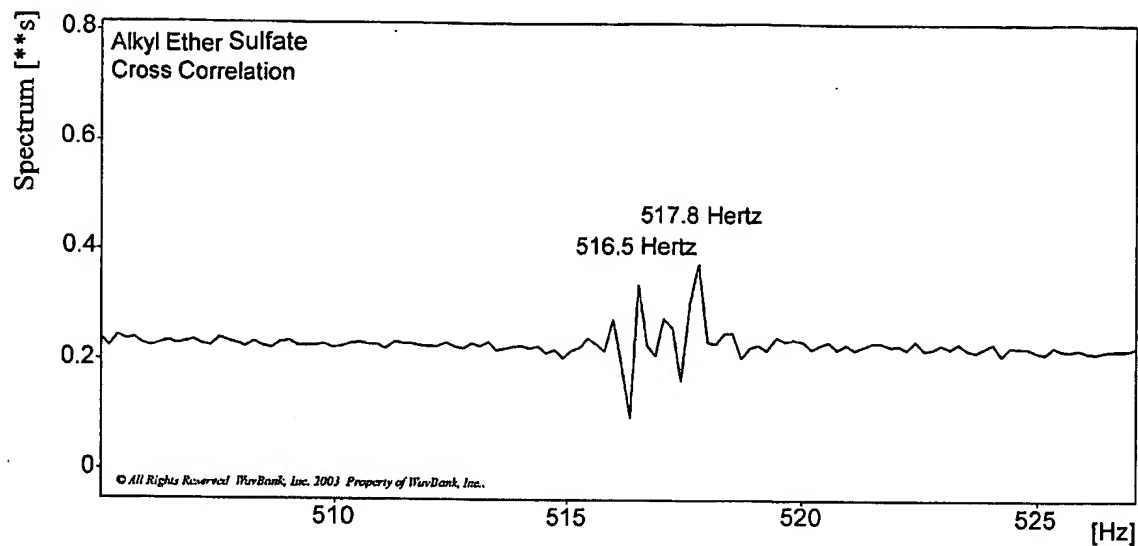
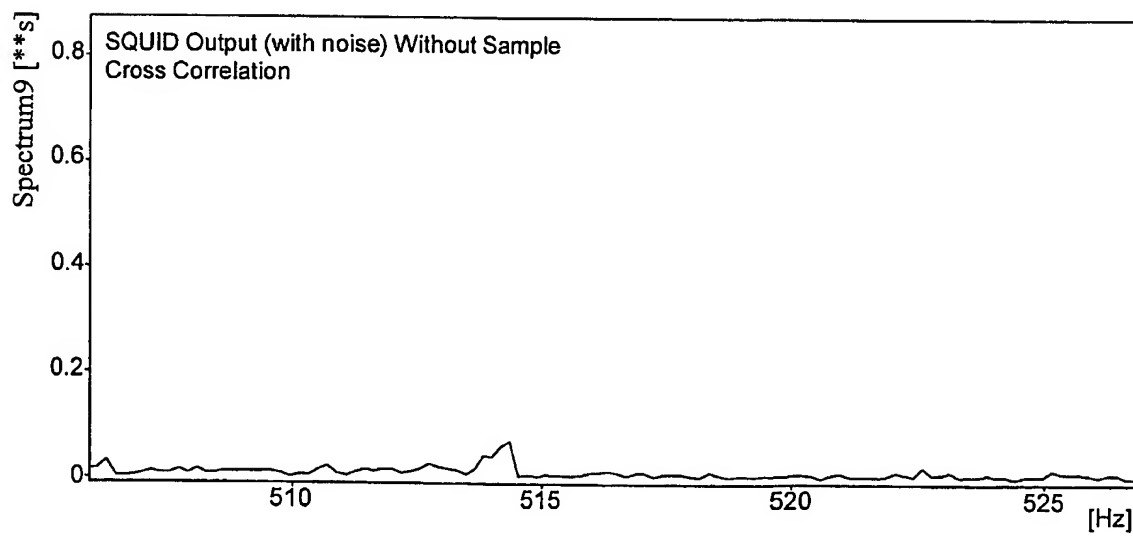
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**FIG. 14A****FIG. 14B**

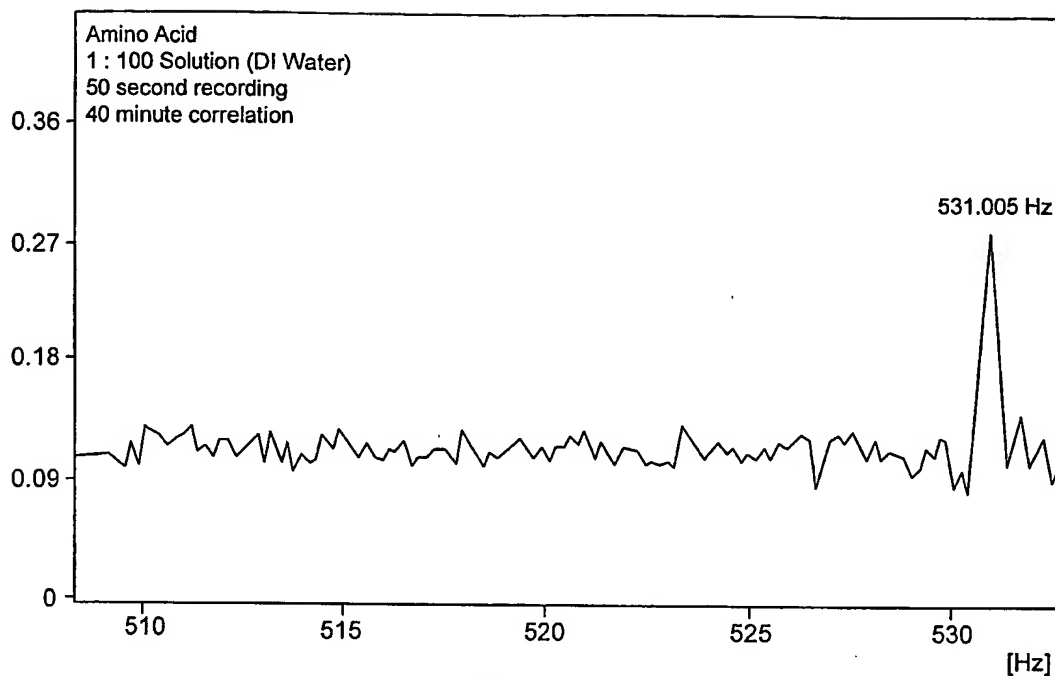
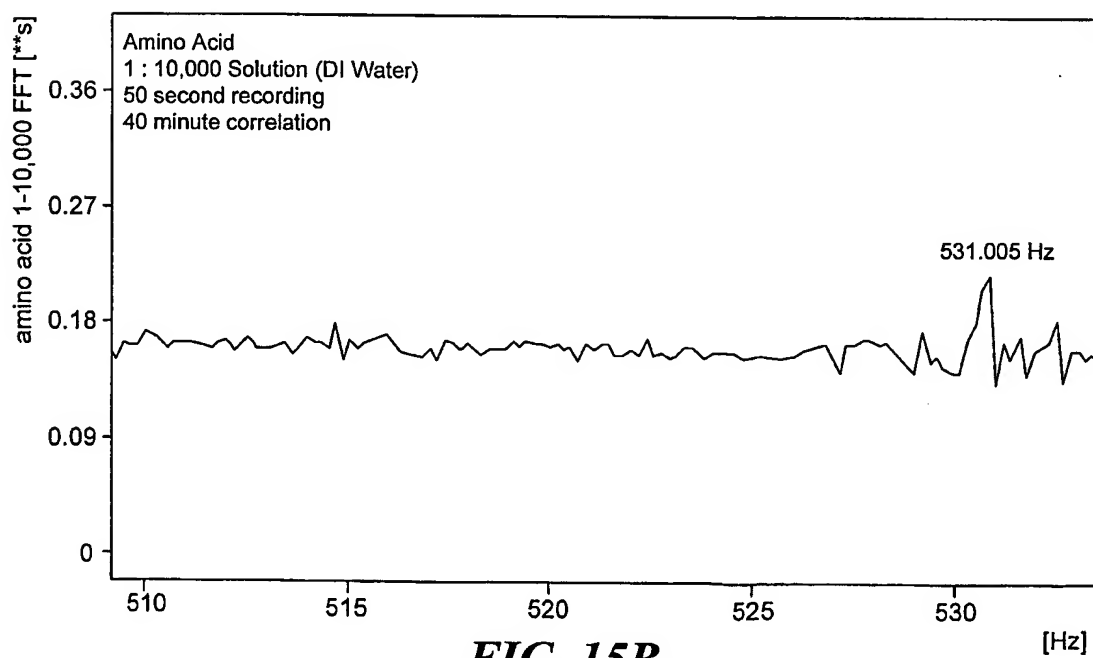
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*FIG. 14C**FIG. 14D*

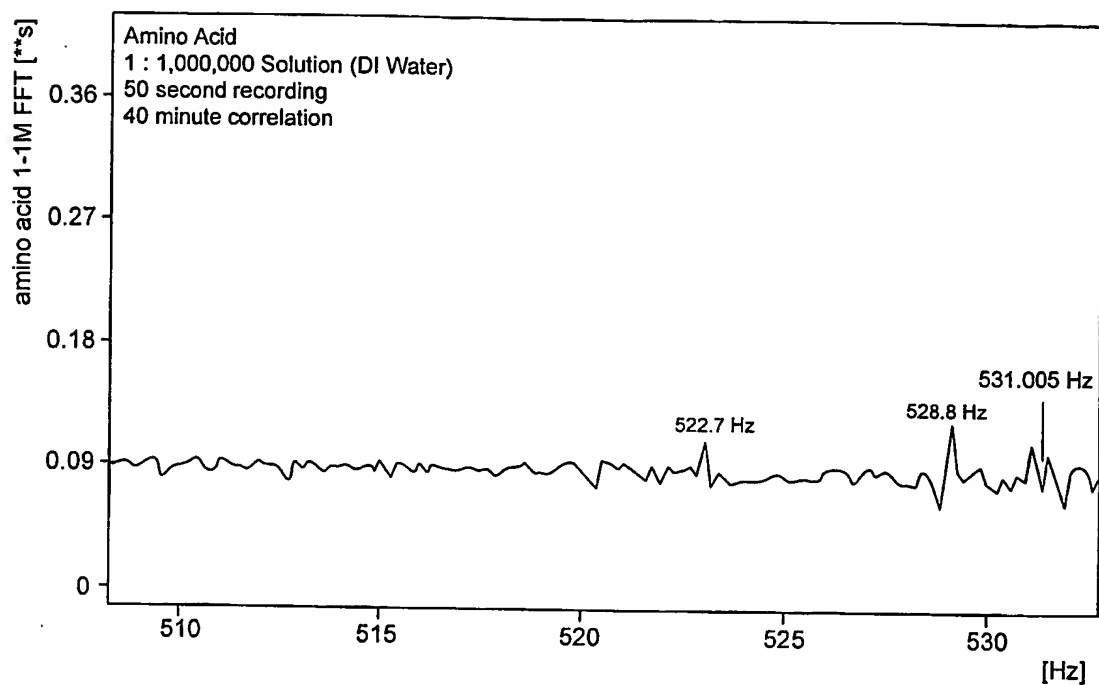
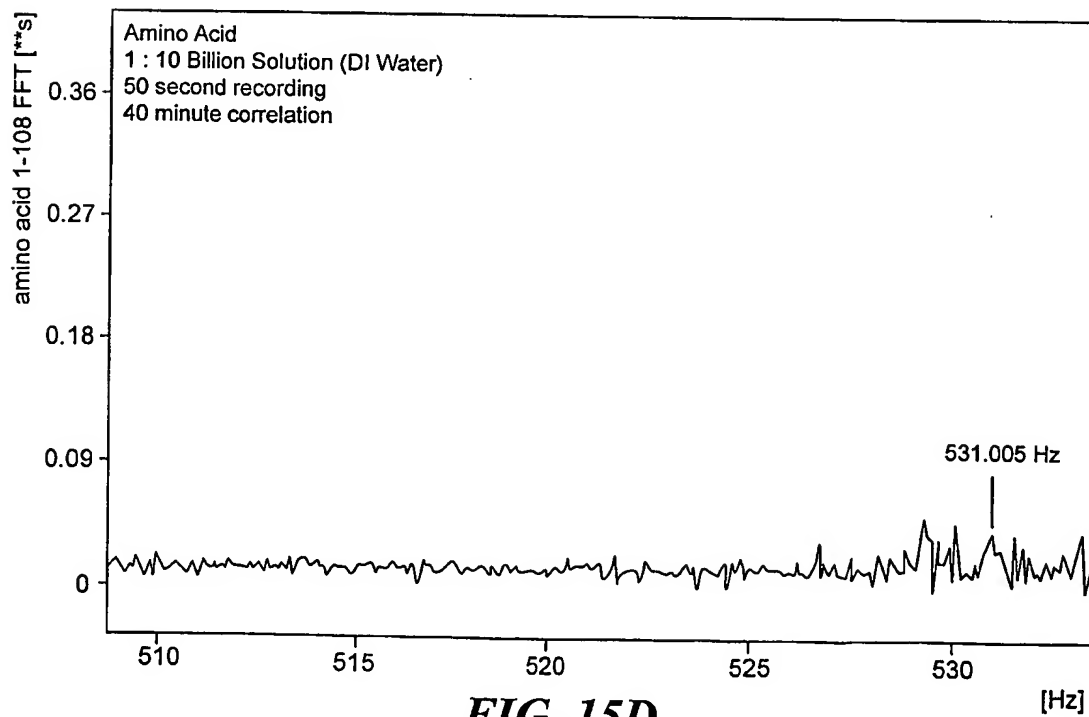
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**FIG. 14E****FIG. 14F**

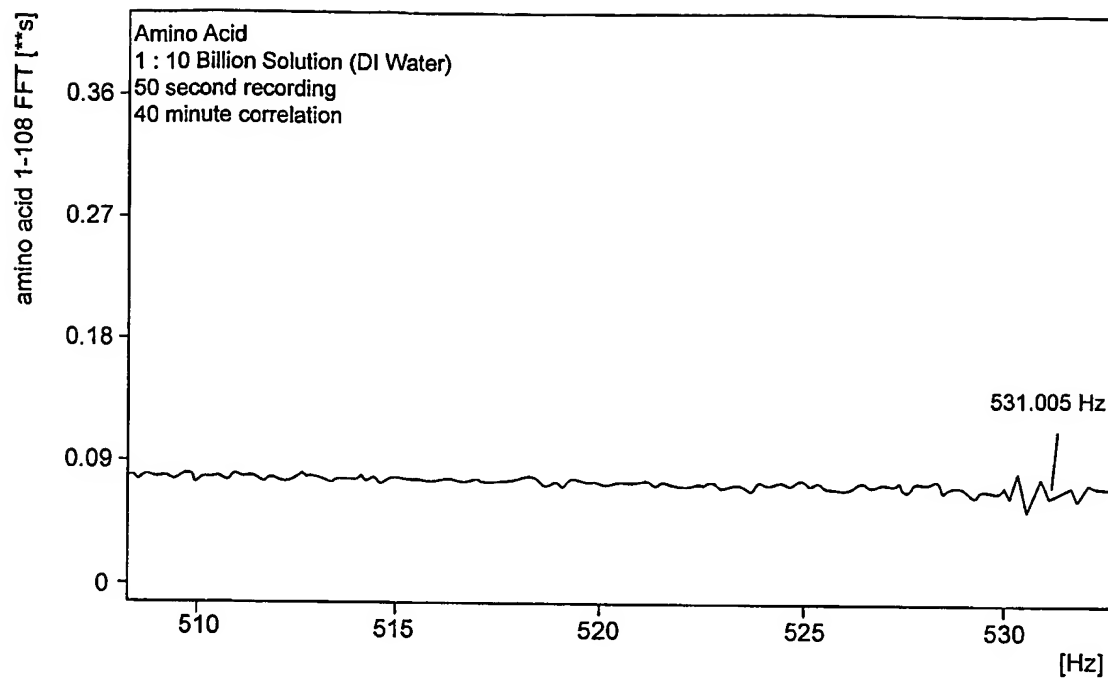
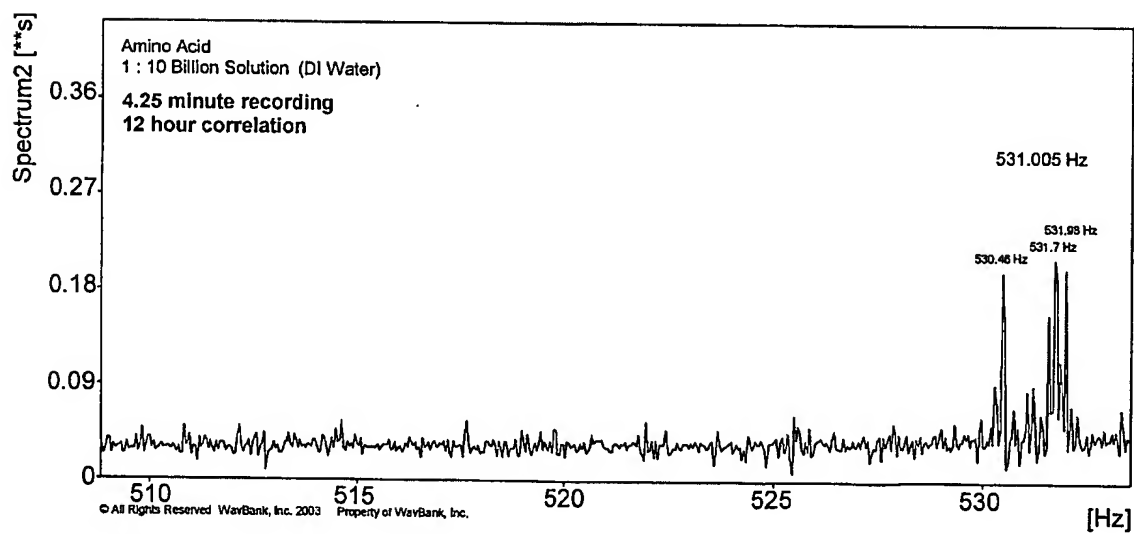
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**FIG. 15A****FIG. 15B**

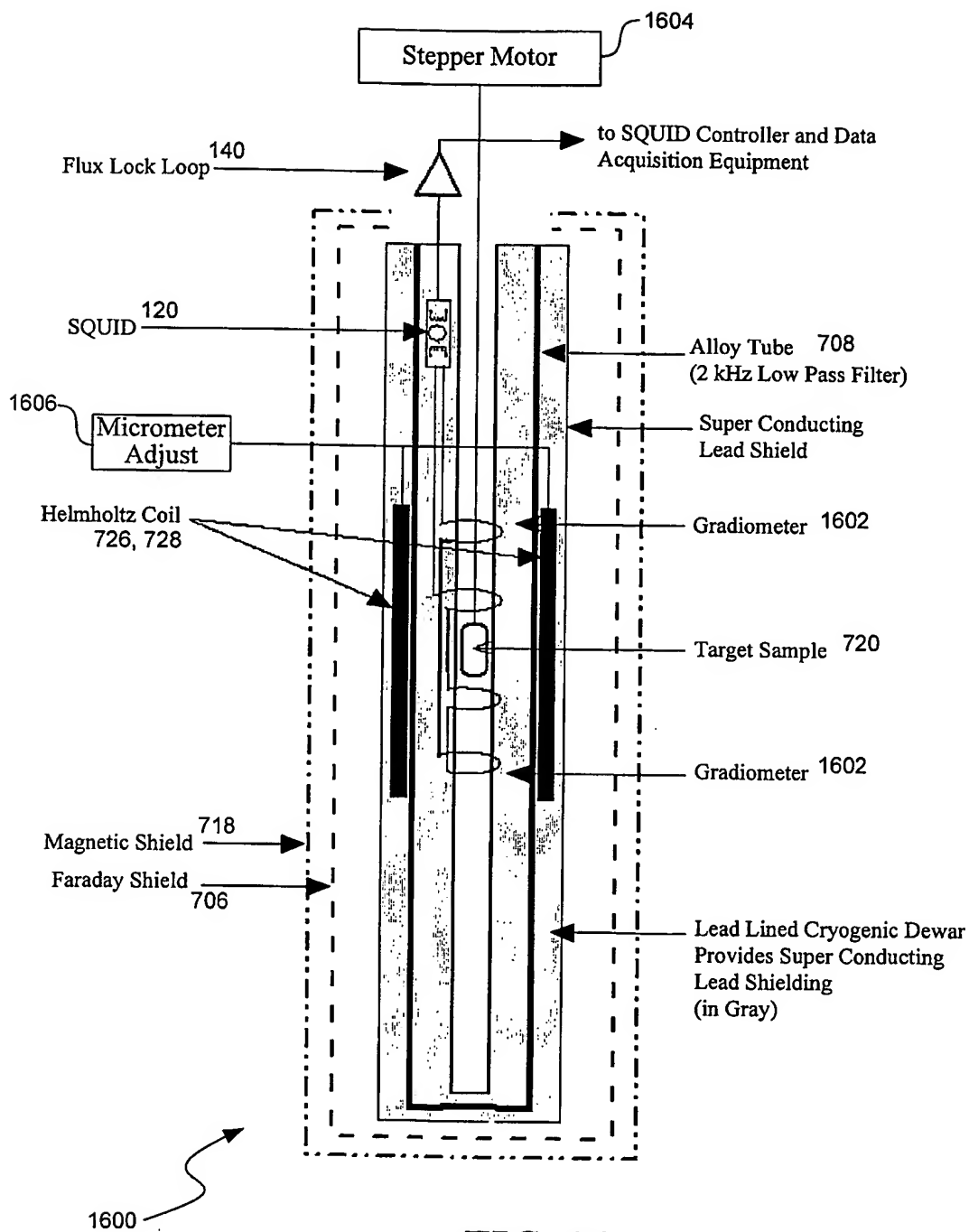
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**FIG. 15C****FIG. 15D**

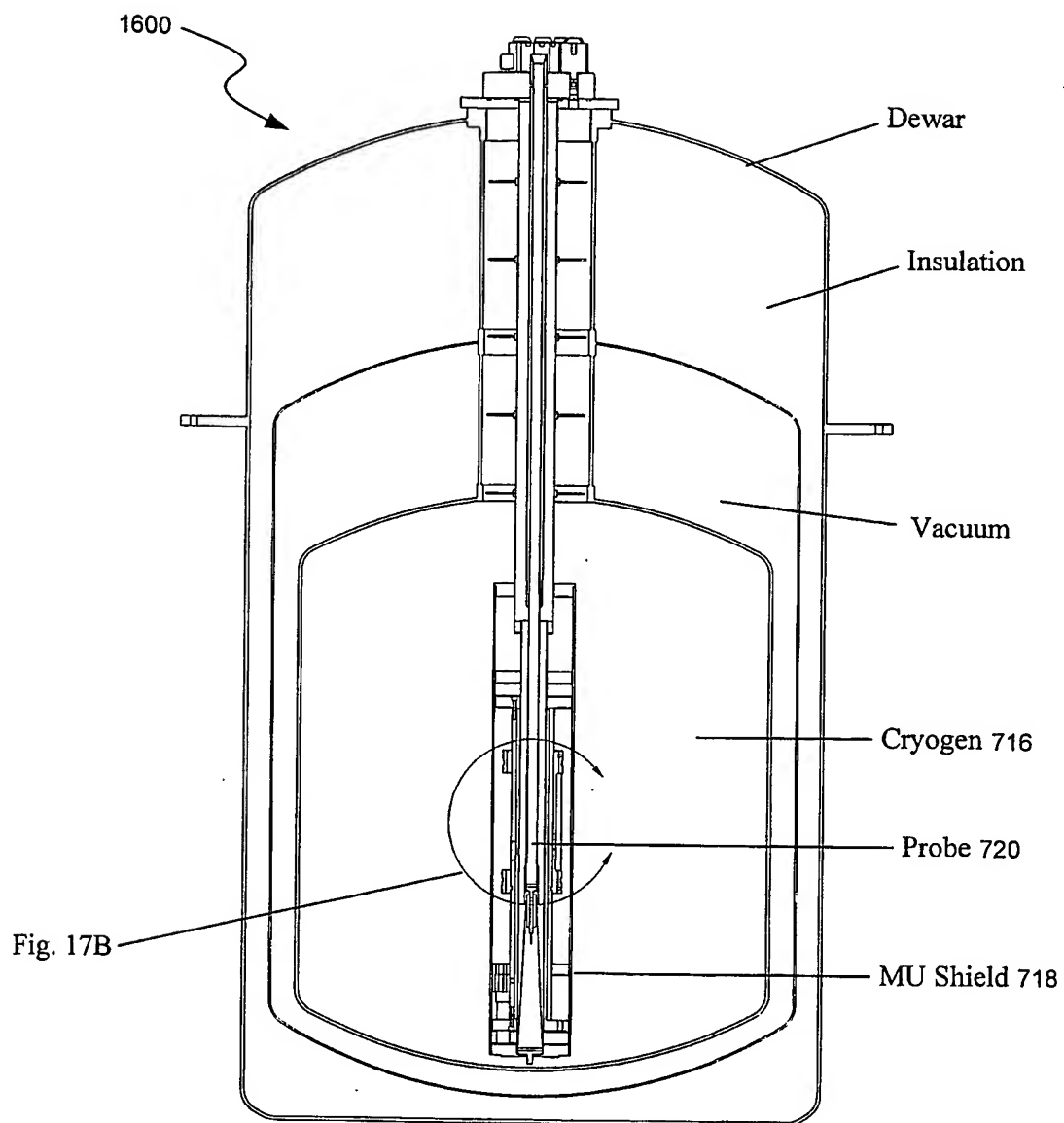
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**FIG. 15E****FIG. 15F**

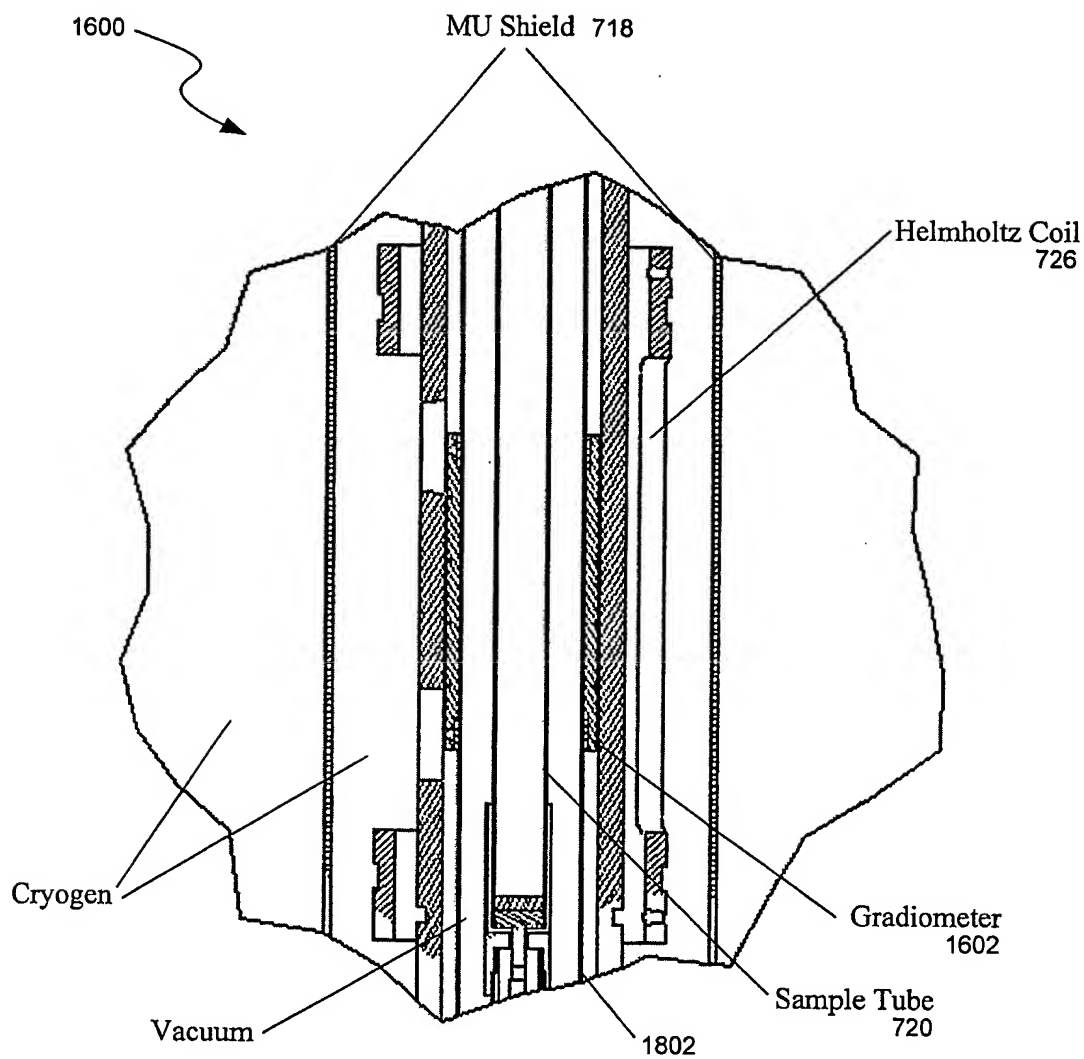
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**FIG. 16**

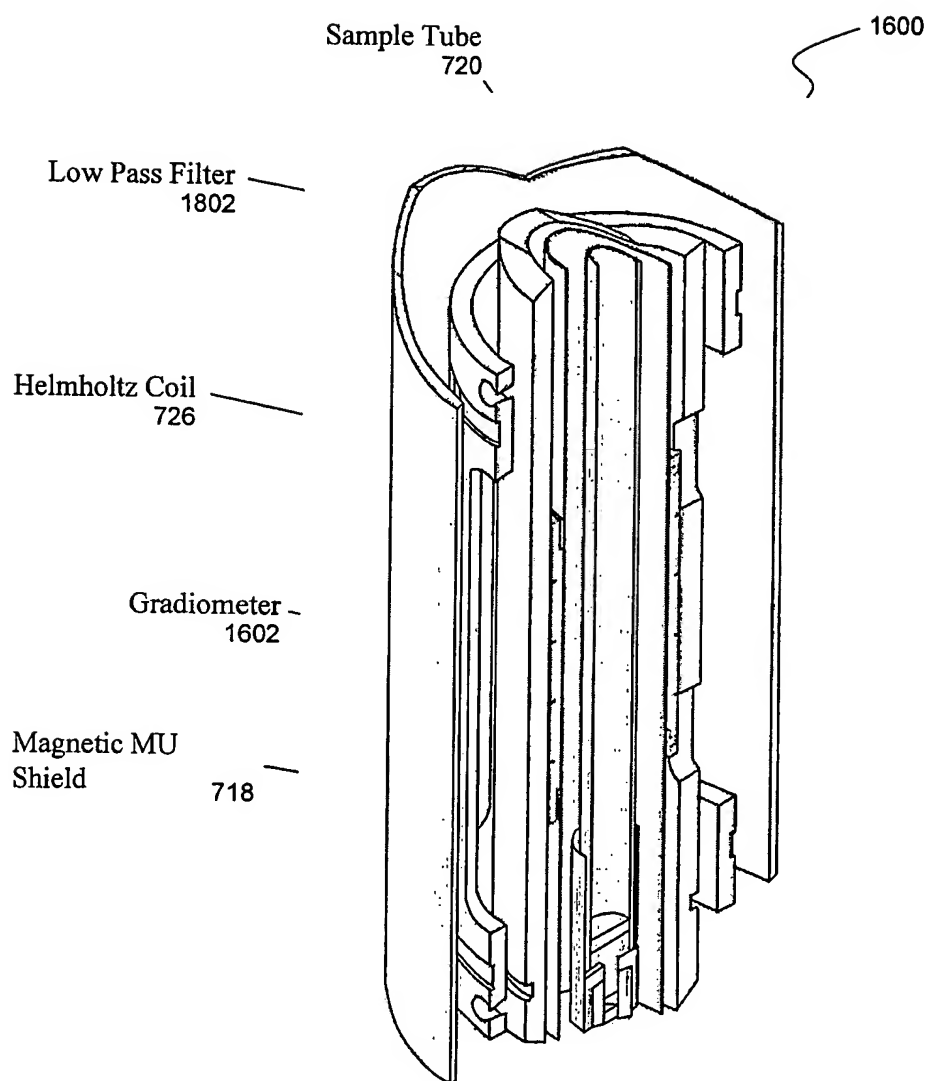
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**FIG. 17A**

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**FIG. 17B**

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**FIG. 18**

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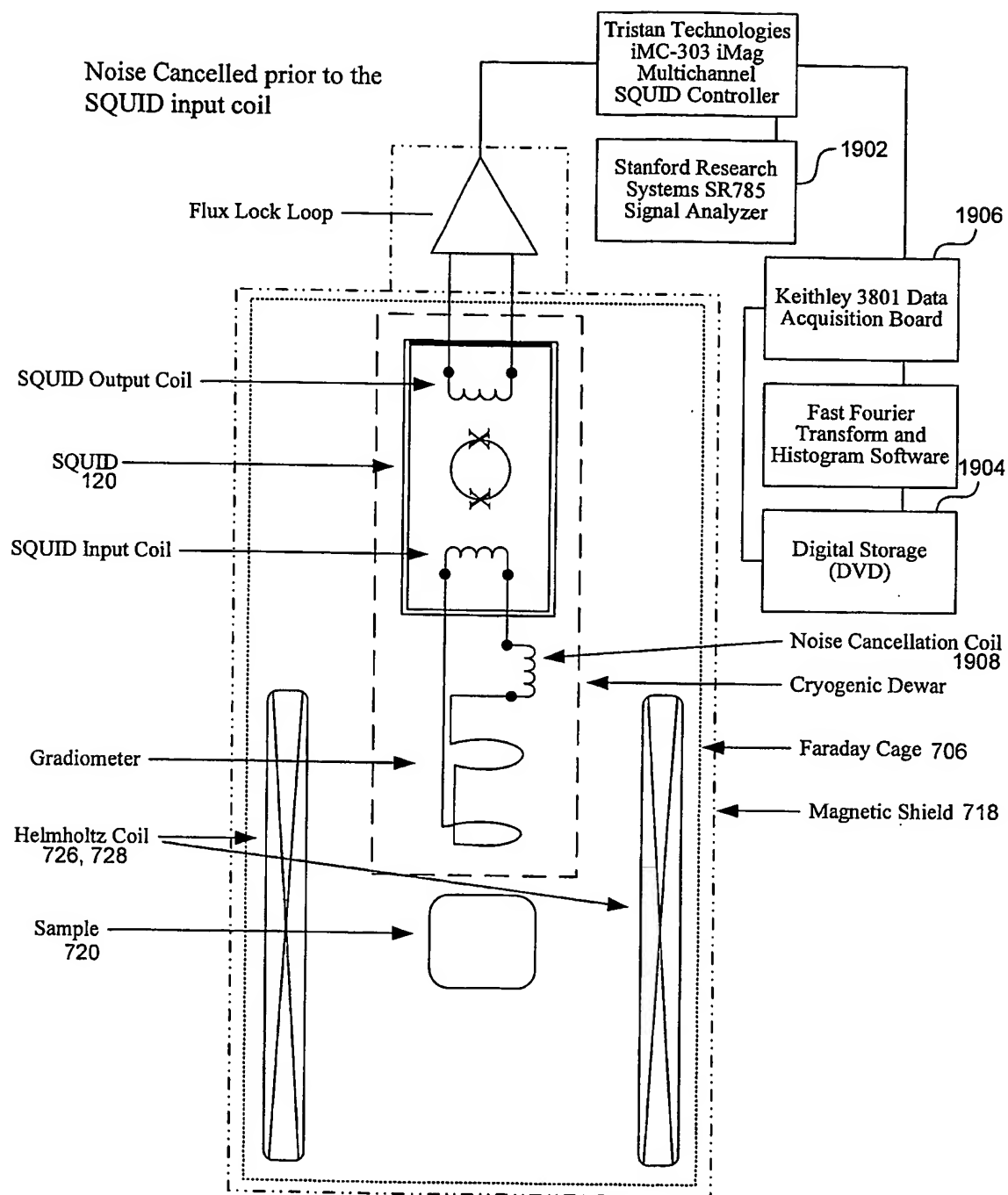
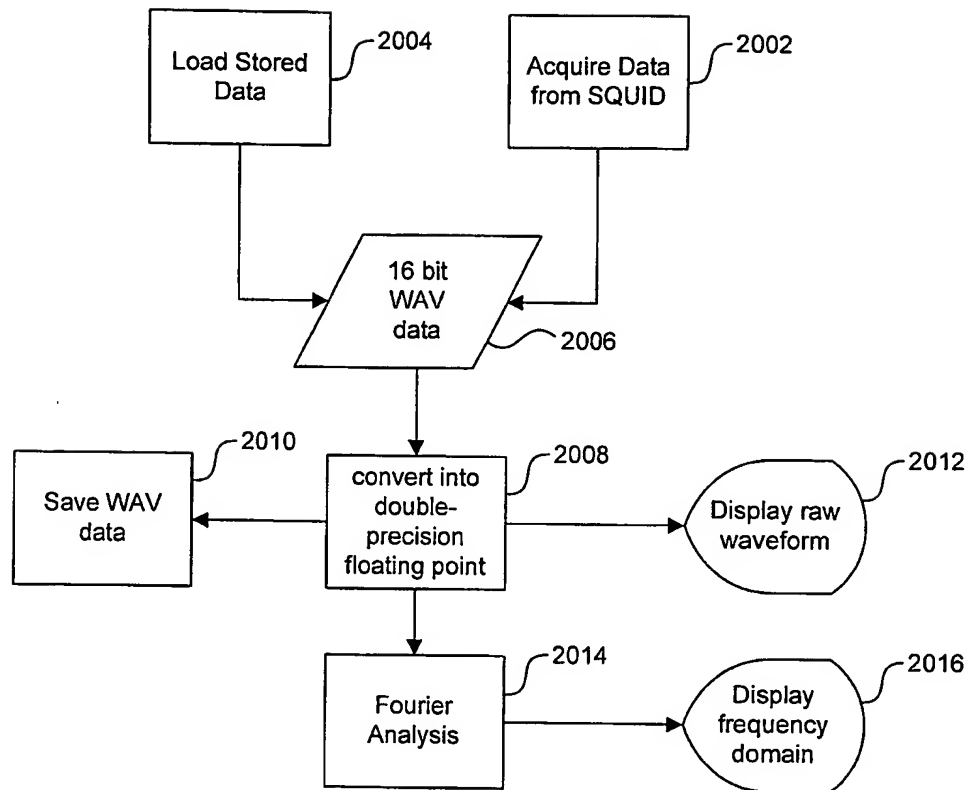


FIG. 19

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**FIG. 20**

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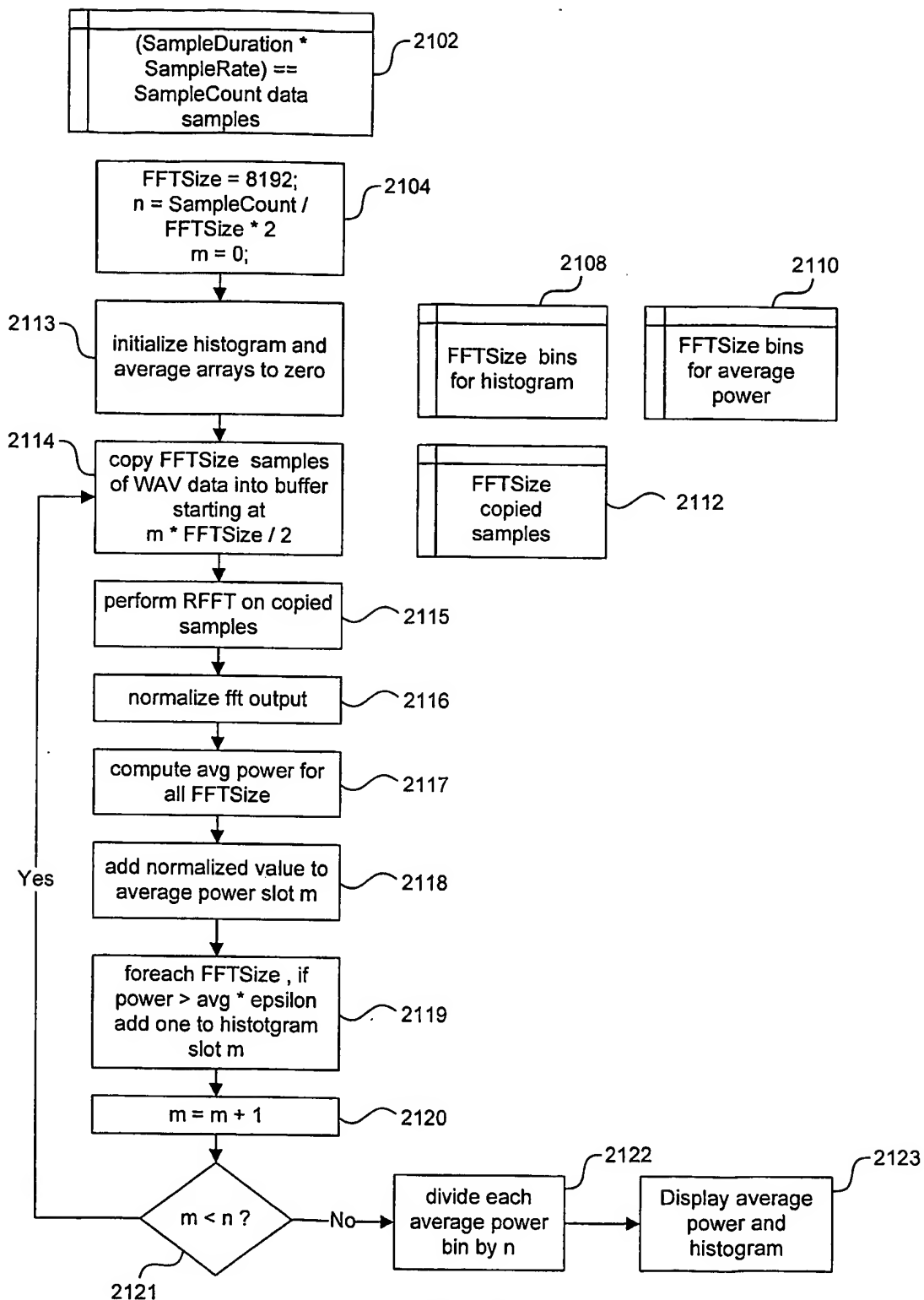
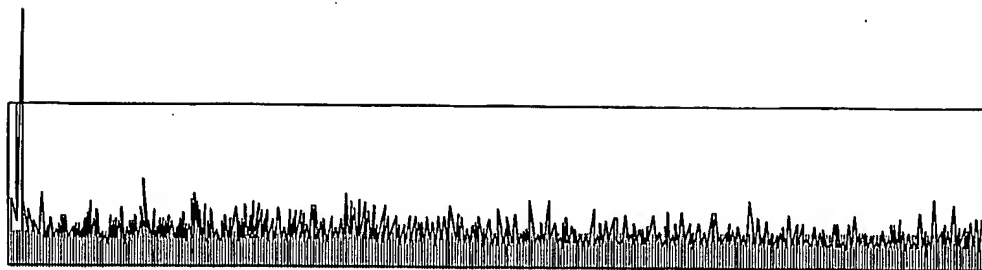


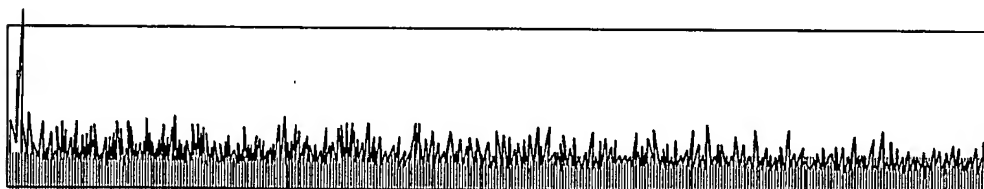
FIG. 21

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400 mV noise signal applied. No stochastic event visible.

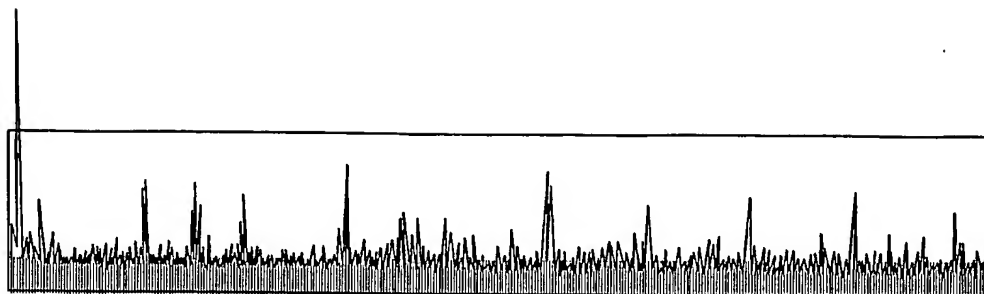
***FIG. 22A***



600 mV noise signal applied. No stochastic event visible.

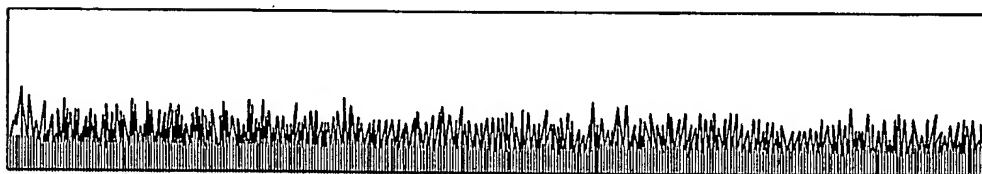
***FIG. 22B***

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700 mV noise signal applied. Stochastic event visible.

***FIG. 22C***



900 mV noise signal applied. No stochastic event visible.

***FIG. 22D***

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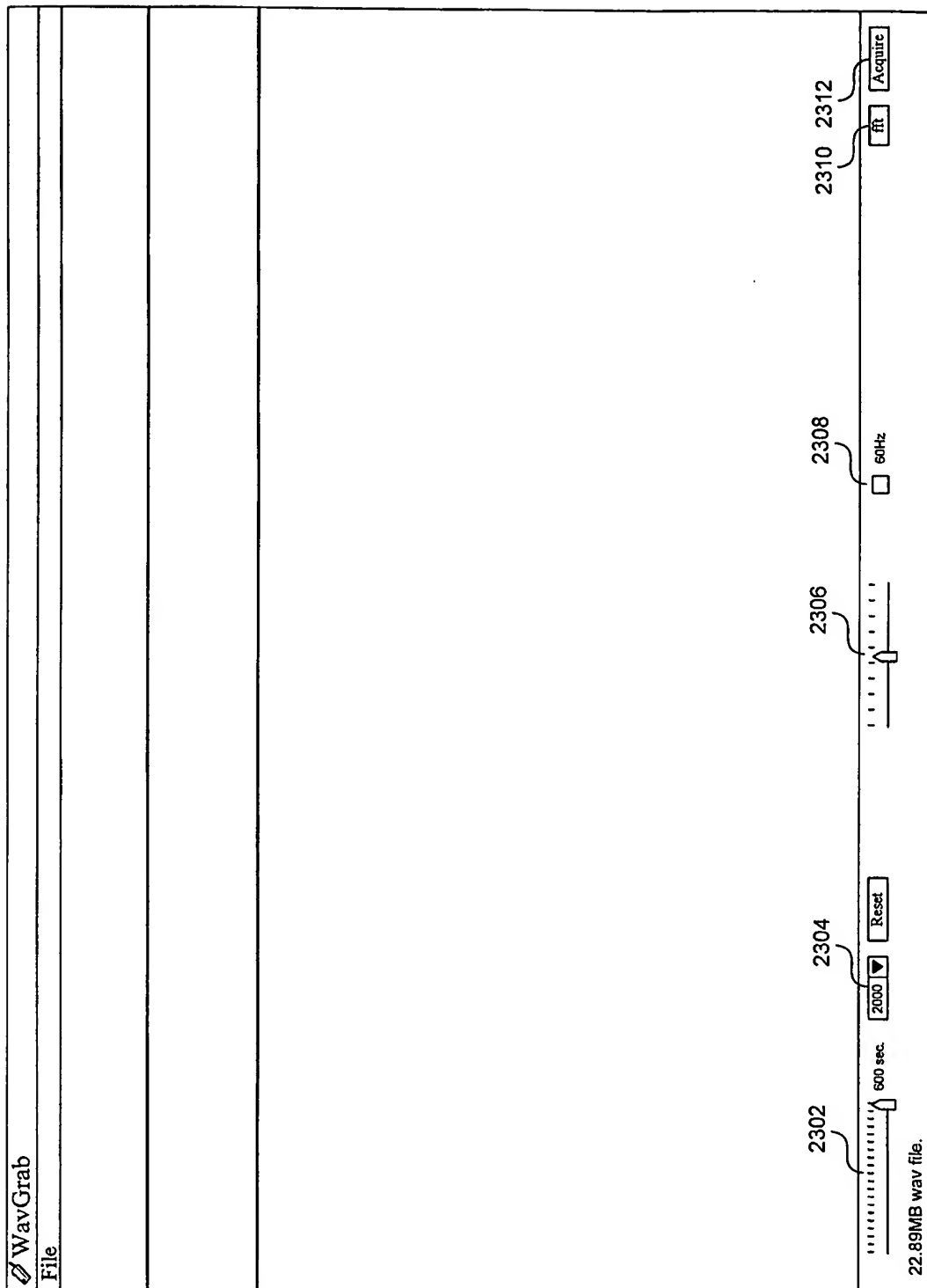


FIG. 23A

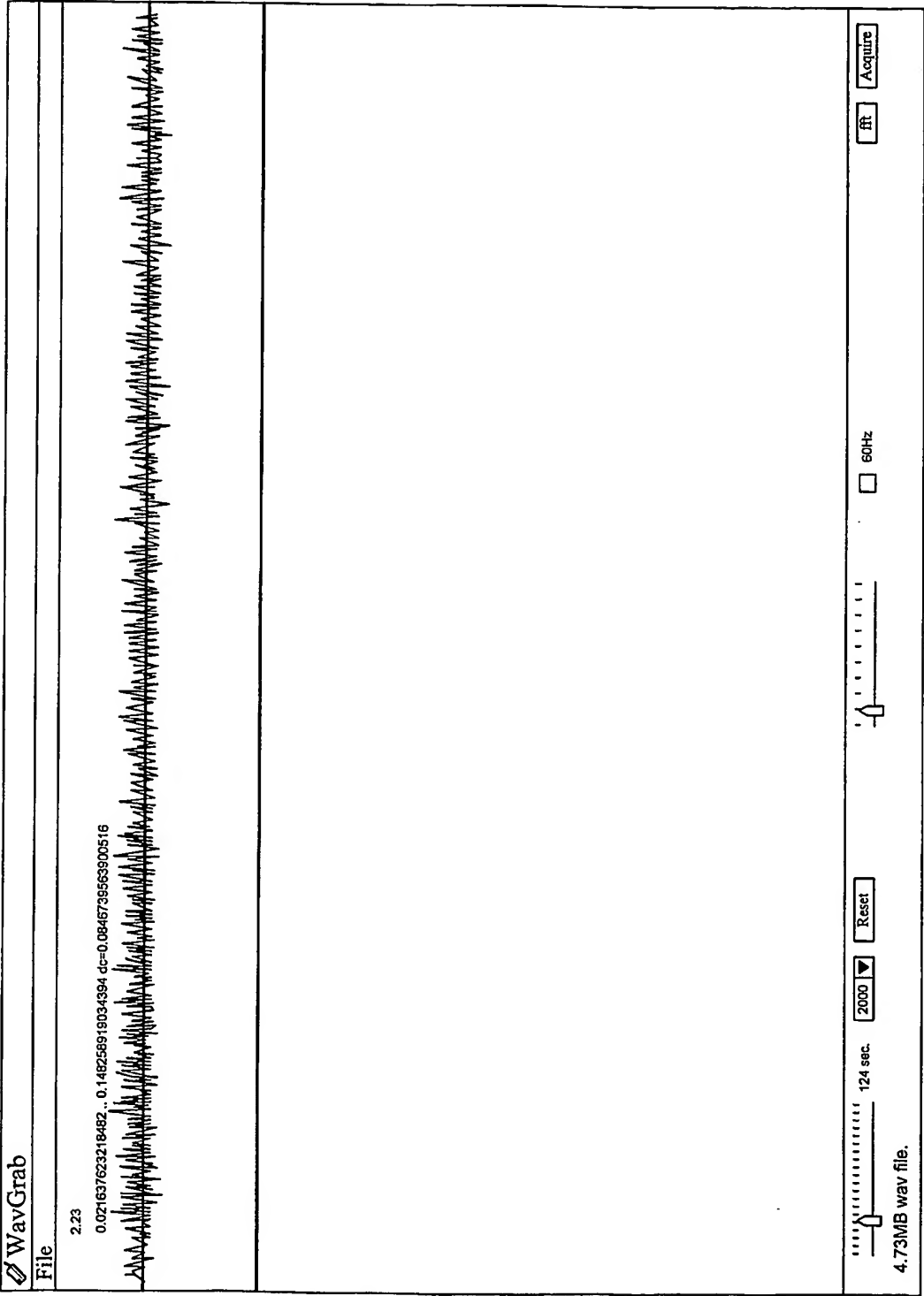


FIG. 23B

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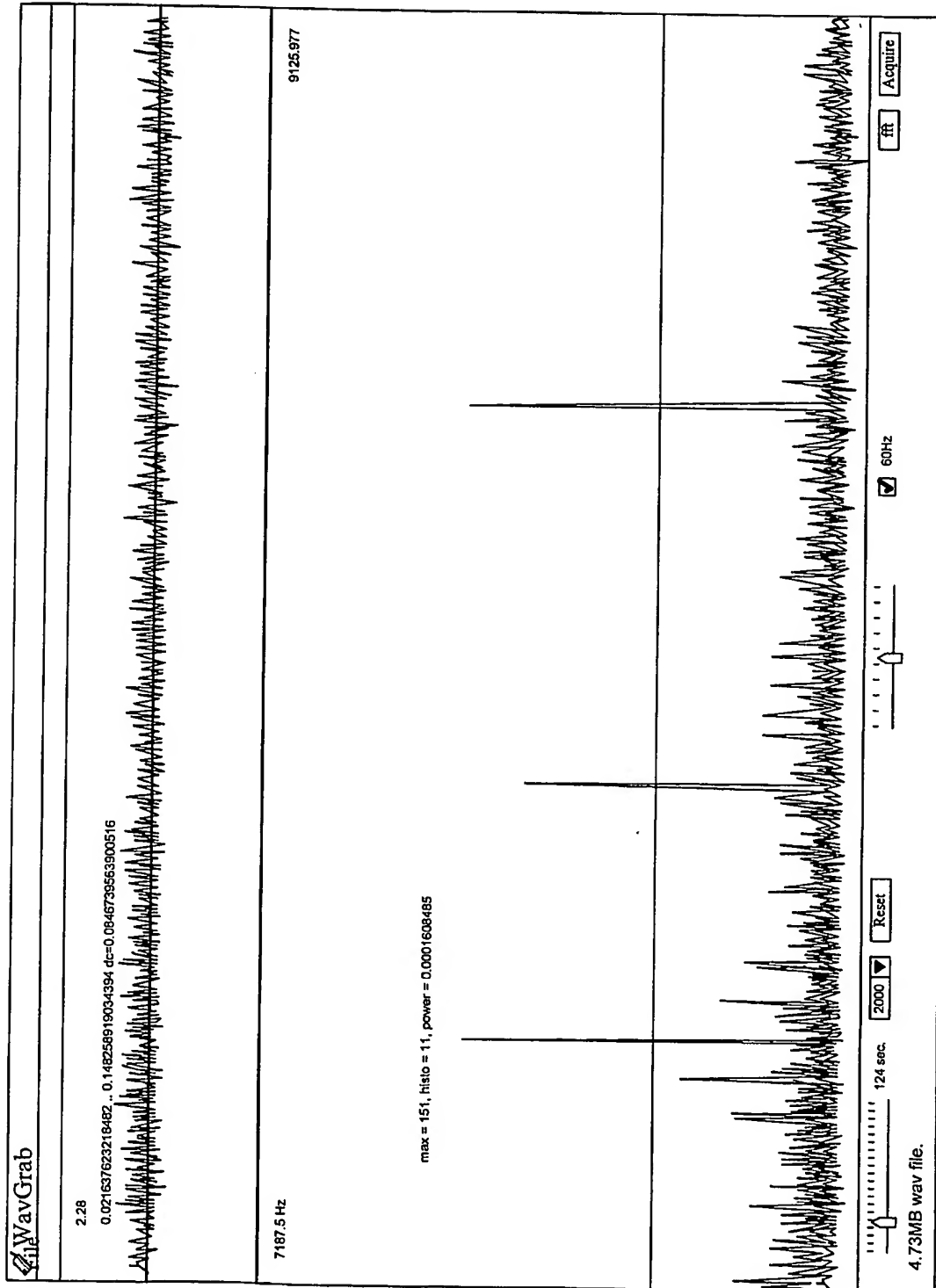


FIG. 23C

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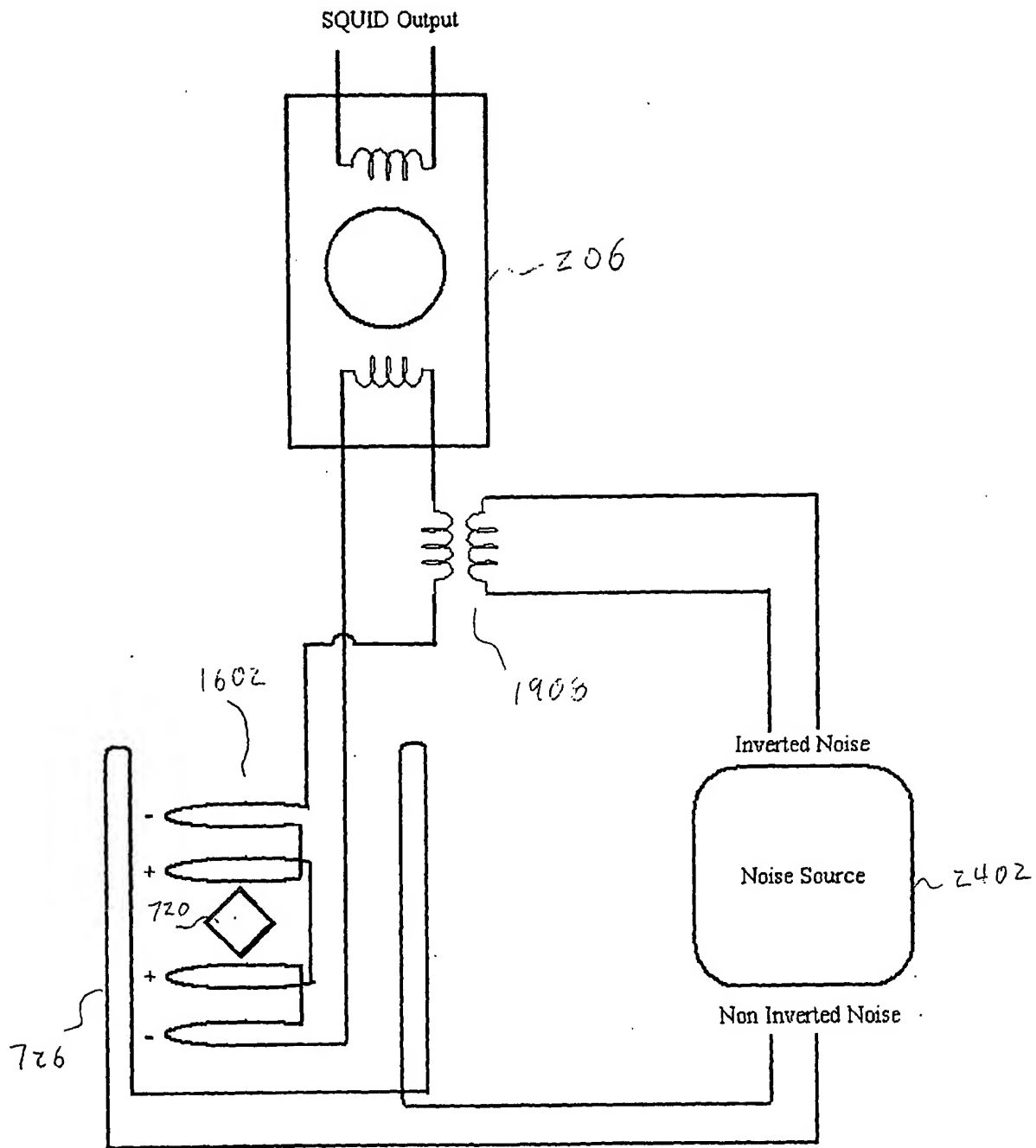


FIG. 34

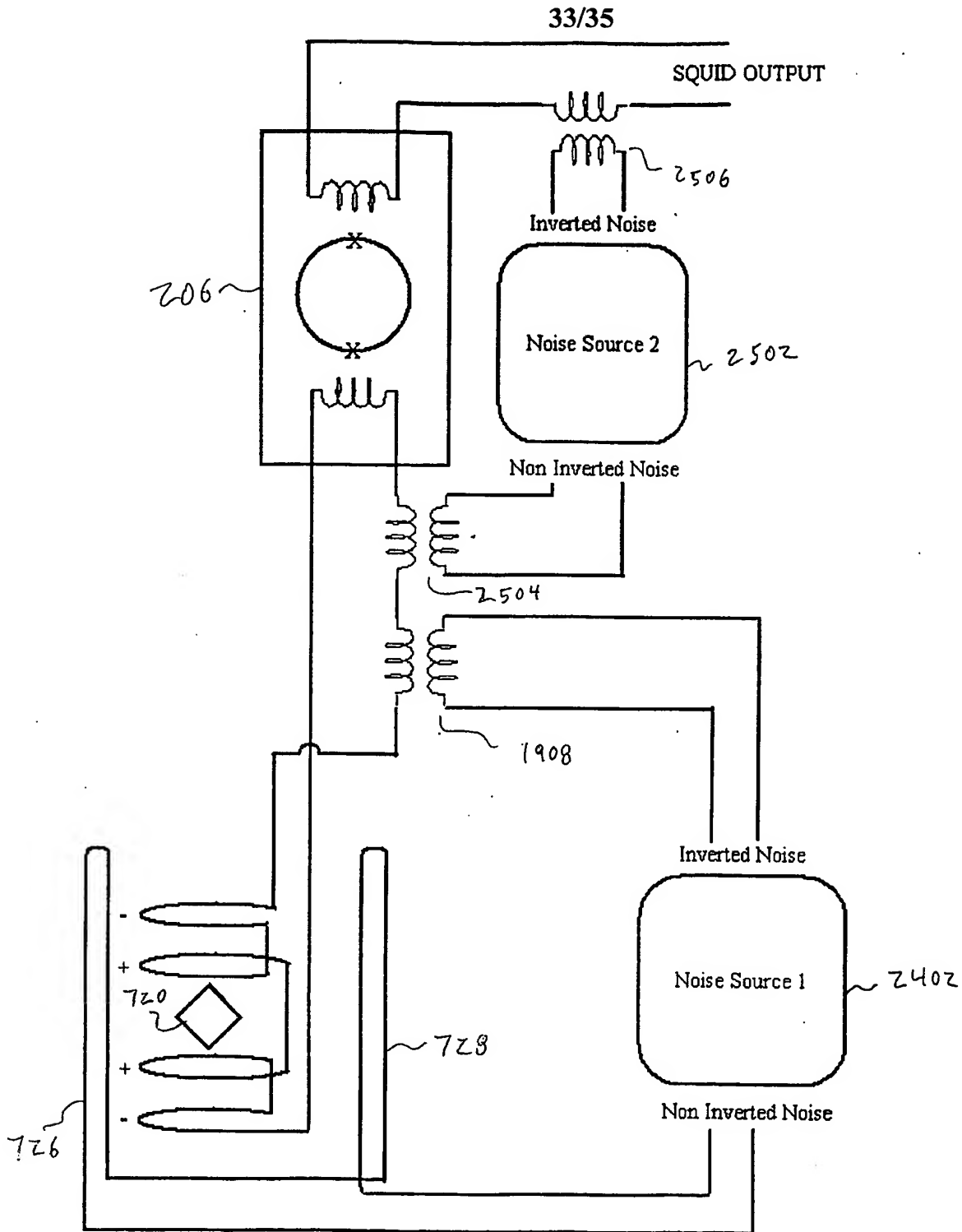


FIG 25

2500

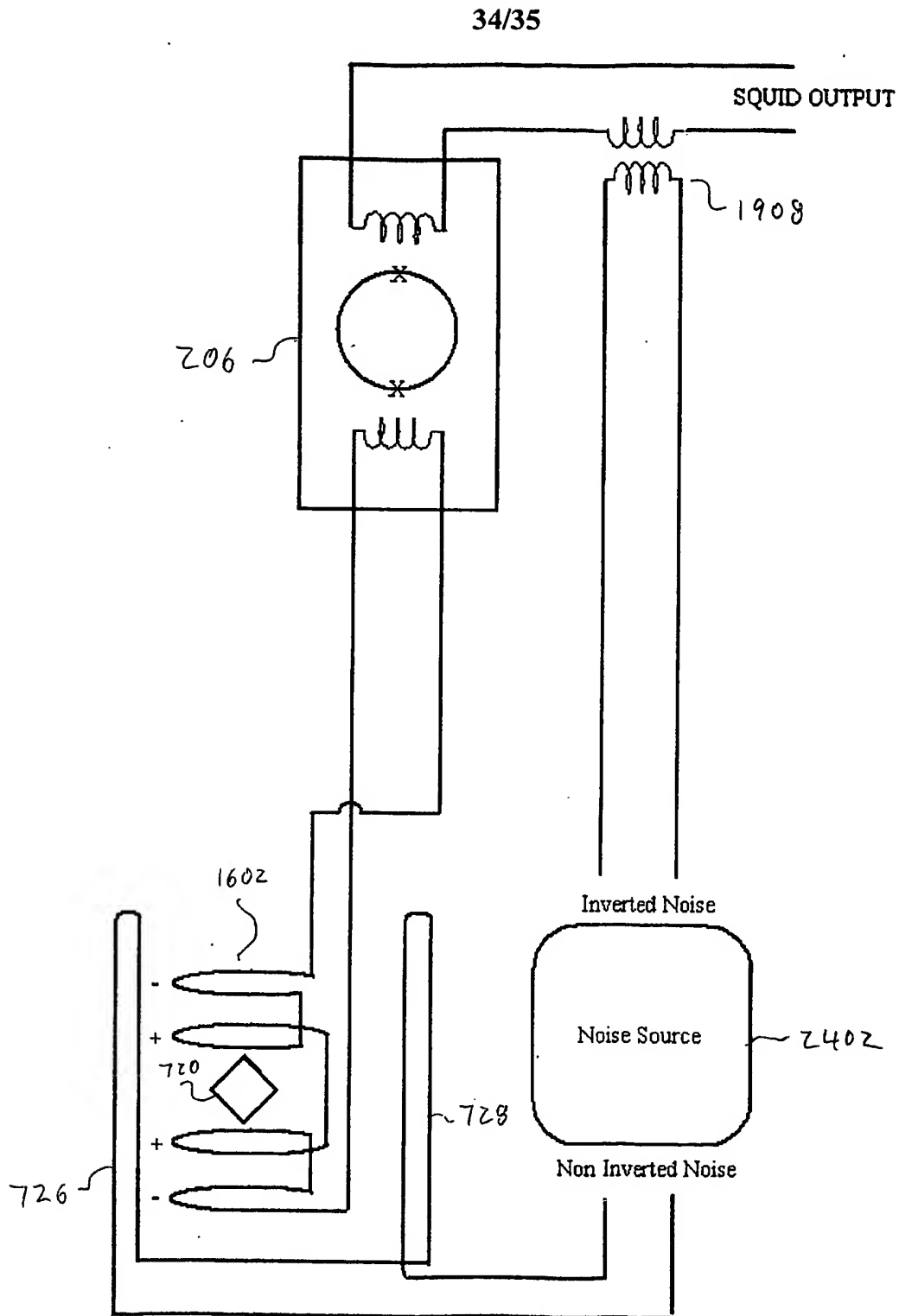


FIG. 26

2600

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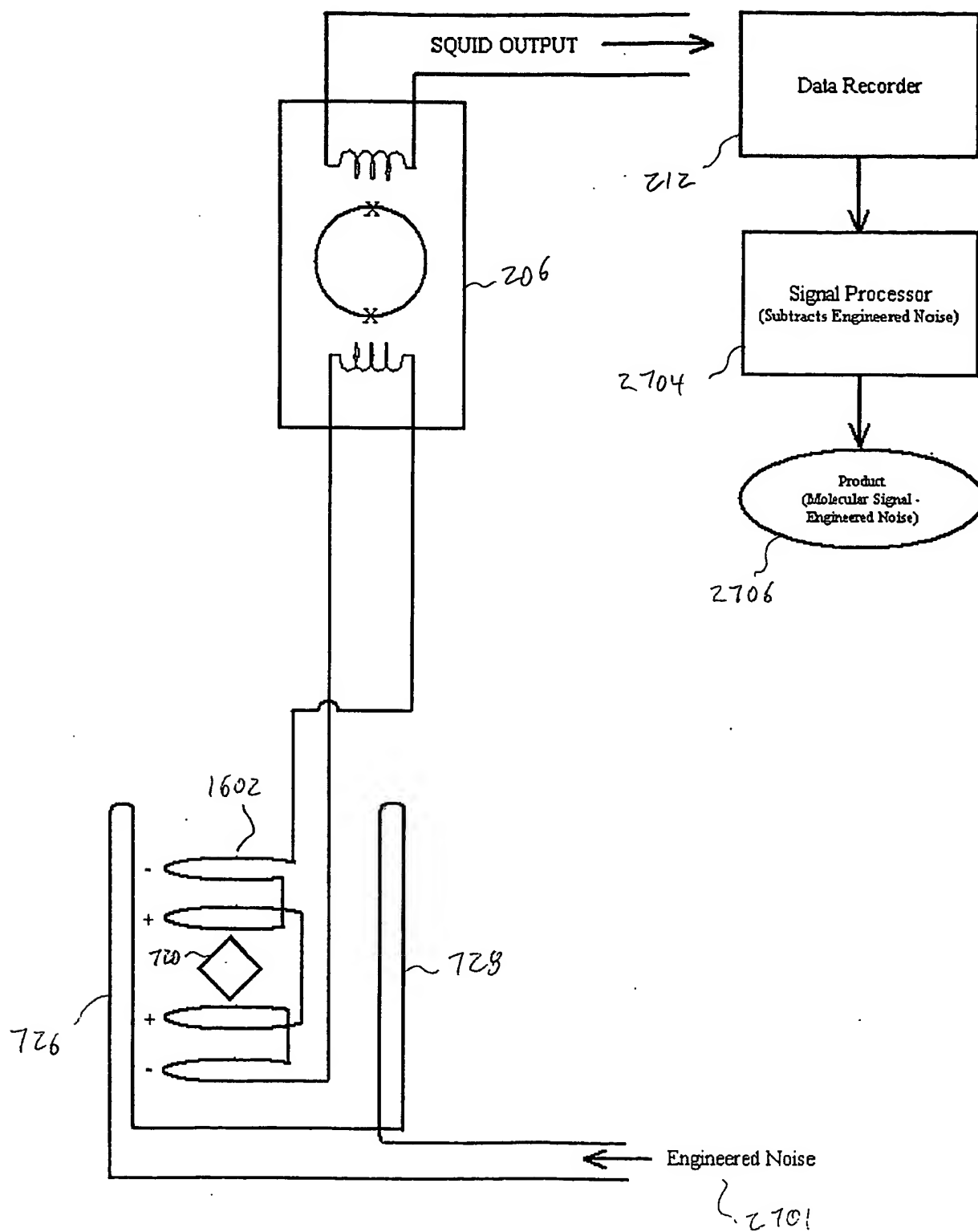


FIG. 27

2700